

ELI-NP Summer school

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HIGH INTENSITY LASERS

Description, issues and state-of-the-art

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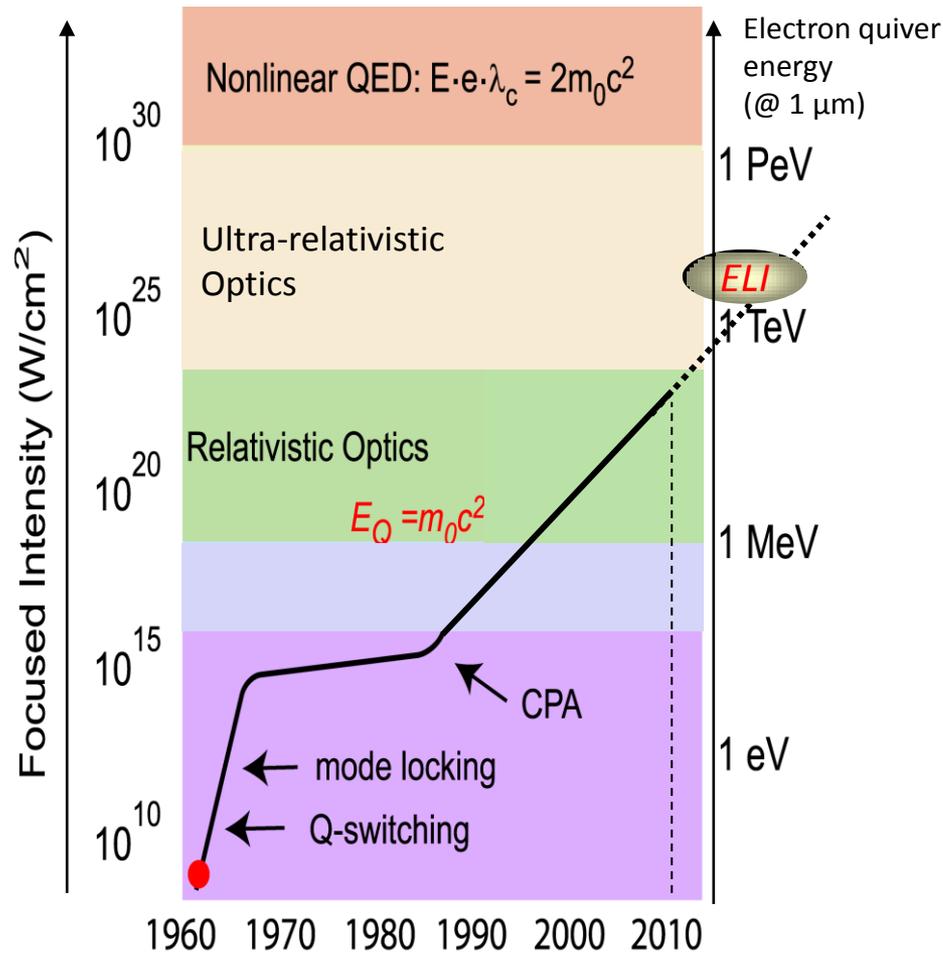
General description of high intensity laser system

Measurement tools

Issues relative to energy, temporal and spatial domains

World-wide State-of-the-art

The interest for ultra-intense lasers



Very motivating fields of physics
To be explored such as
Particles acceleration (e^- , hadrons), HHG,
Table-top X-rays, Gamma rays

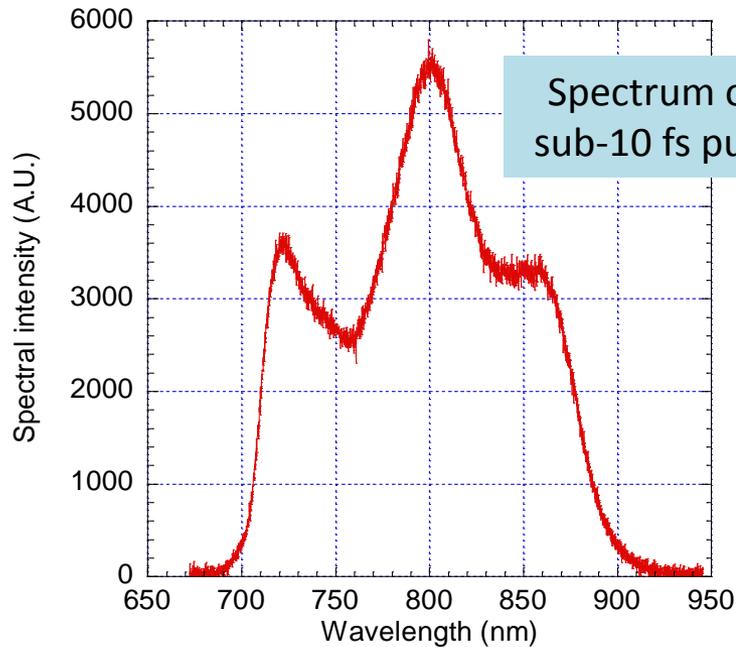
First application of fs pulses
Has been in ophthalmology for
Cornea surgery

A femtosecond pulse

As the pulse is short, the laser beam is no more monochromatic

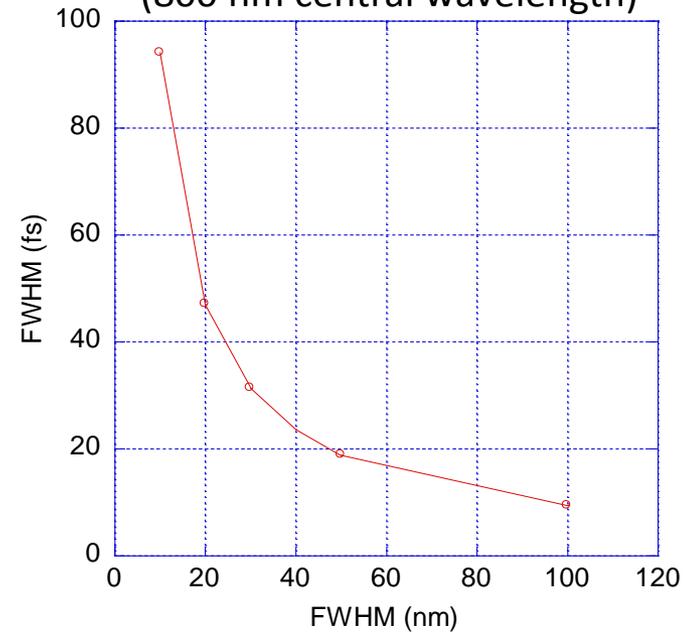
$$\Delta T_{1/2} \Delta \nu_{1/2} = k$$

k = 1 for rectangular
k = 0.441 for a Gaussian



FFT calculation required

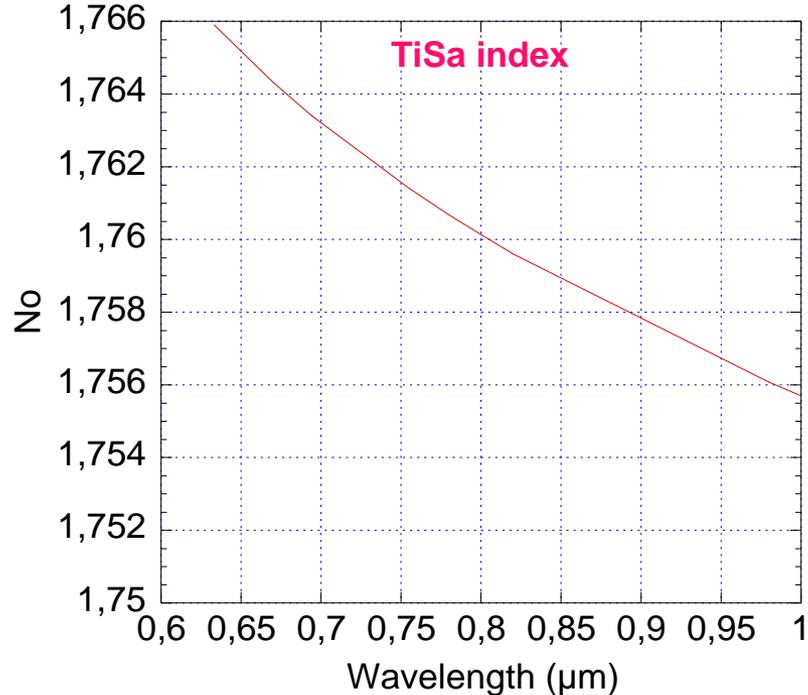
Spectral to Time domain relation
(800 nm central wavelength)



$$\Delta T_{1/2} = \frac{0.441 * \lambda^2}{c * \Delta \lambda_{1/2}}$$

The dispersion

Refractive index is changing with the wavelength



$$\phi(\omega) = \phi_0 + \phi^{(1)}\Omega + \frac{1}{2}\phi^{(2)}\Omega^2 + \frac{1}{6}\phi^{(3)}\Omega^3 + \dots$$

$$\Omega = \omega - \omega_0$$

For a pulse with Gaussian shape

$$\Delta T = \Delta T_0 \sqrt{1 + \frac{16(\ln 2)^2 \phi^{(2)2}}{\Delta T_0^4}}$$

For 1cm TiSa crystal, the pulse duration lengthening is

30 fs \Rightarrow 62 fs

20 fs \Rightarrow 81.8 fs

10 fs \Rightarrow 159.6 fs

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How to amplify the femtosecond pulses?

Femtosecond pulses (10^{-15} s)

- ⇒ Small amount of energy leads to high intensity
- ⇒ Non linear effect or optical breakdown and damage

⇒ 100 μ J in 20 fs on 200 μ m spot size gives an intensity of $1.5 \cdot 10^{13}$ W/cm²

- ⇒ Non linear effects occurs, that will destroy the beam quality in time and space
- => Optical breakdown on the optical surface of components that causes damage

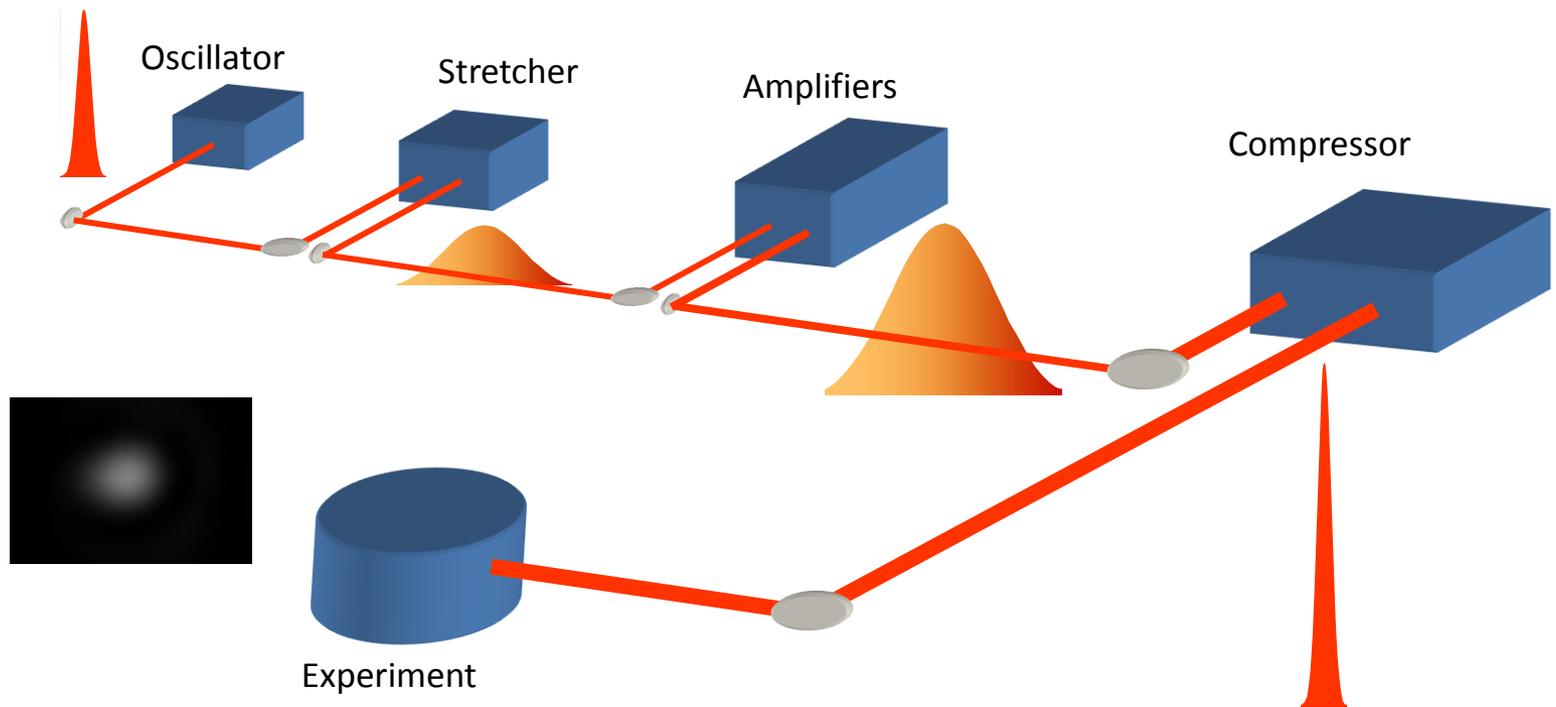
The solution is to lengthen the pulse duration while keeping a large spectrum

The CPA concept



The basics scheme has been introduced in 1985 by
Gérard Mourou and Dona Strickland

Donna STRICKLAND et Gérard MOUROU
Compression of amplified chirped optical pulses
Opt. Com., Vol 56, number 3, 1 December 1985



Simple scheme but with drawbacks for High energy and short pulse lasers

The generation of femtosecond pulses

The standard generation of fs pulses (Ti:Sa, Yb doped):

The goal is to exploit the largest spectral bandwidth (Femtolasers, Venteon, Spectra-Physics, Coherent, KMLabs, Amplitude Systems, JDSU previously Time Bandwidth...)

Average power: up to 1W

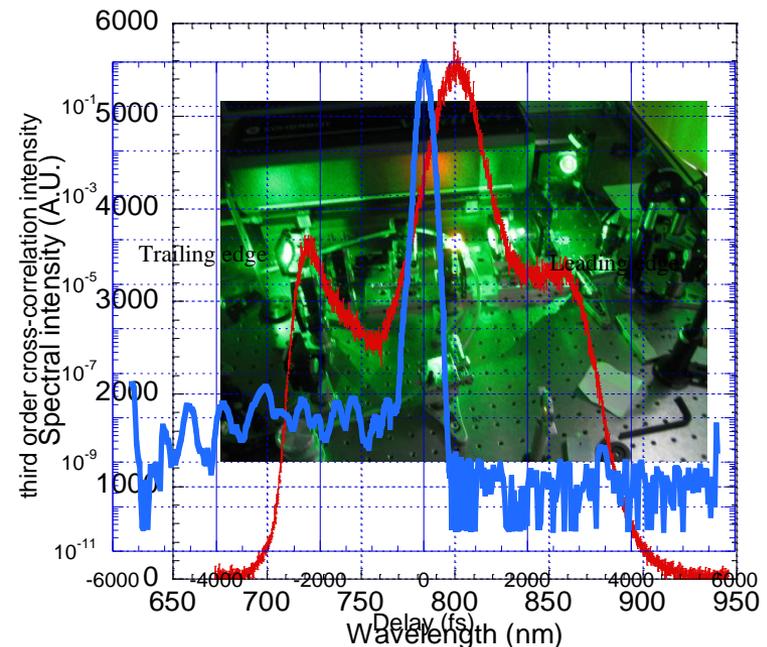
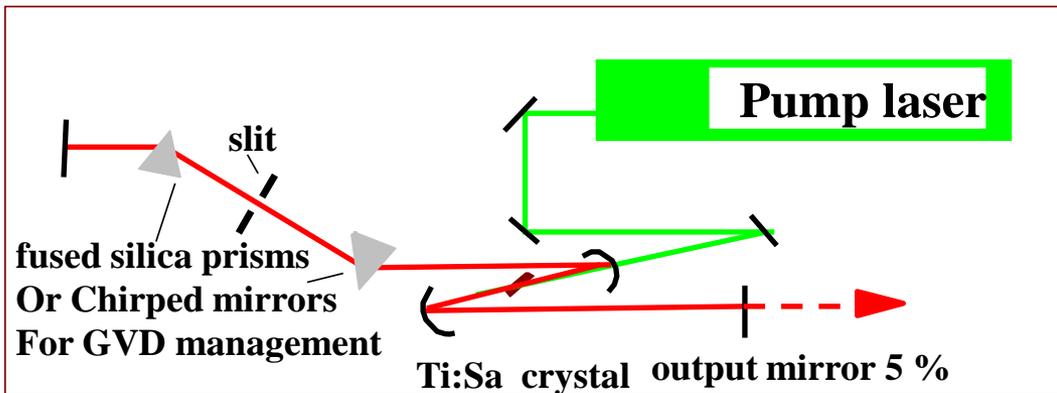
Pulse duration: as short as 5 fs

Water cooling

In a laser cavity, Kerr lens mode-locked:

Balance between intra-cavity intensity for non-linear effects and GVD

High temporal contrast => "ideal" for seeding amplifiers



Stretching the seed pulse

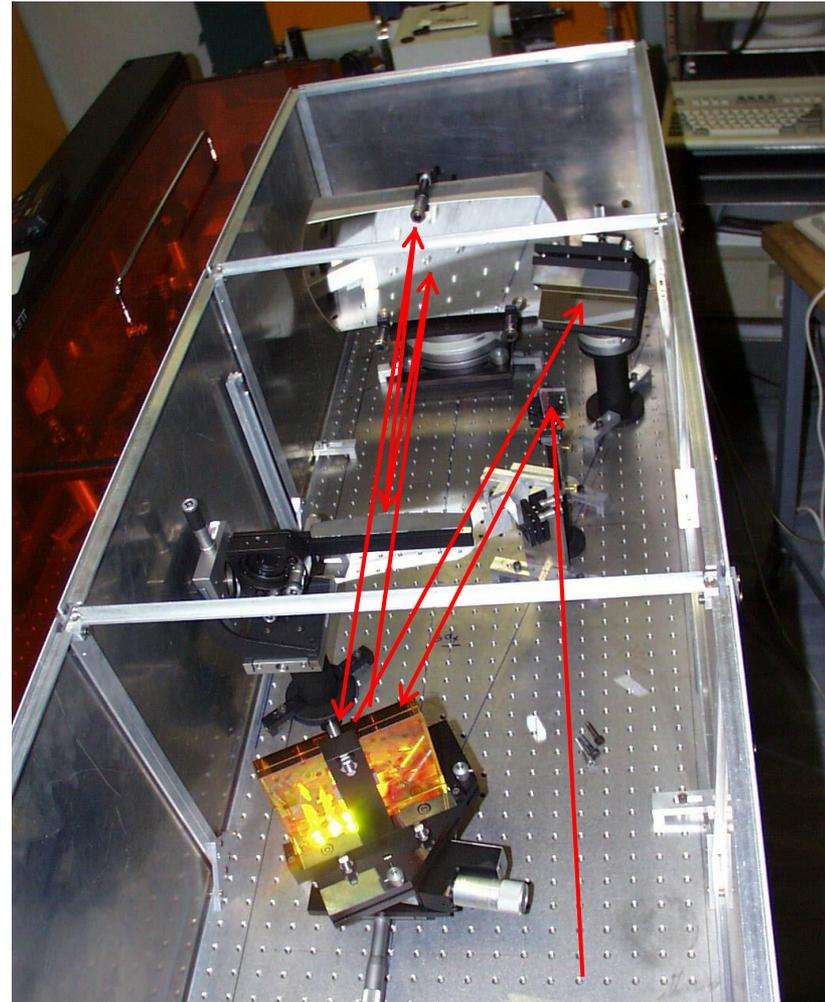
The ways to stretch the laser pulses

- Fibers
- Grating and optical system
- Grisms
- Volume Bragg Gratings

$$\Delta T = \frac{\phi^{(2)} 4 \ln 2}{\Delta T_0} \quad / \quad \phi^{(2)}_{stret}(\omega_0) = \frac{L_{stret} \lambda^3}{\pi c^2 d^2 \cos^2 \theta}$$

For high-intensity lasers, grating based stretcher is the solution

- Öffner type (spherical or cylindrical mirrors) is generally used
- large stretching ratio
- large spectral bandwidth
- very low aberrations



The amplification of femtosecond pulses

In a cavity:

⇒ Regenerative amplifier

Increase the energy to mJ level of the pulse coming from the oscillator

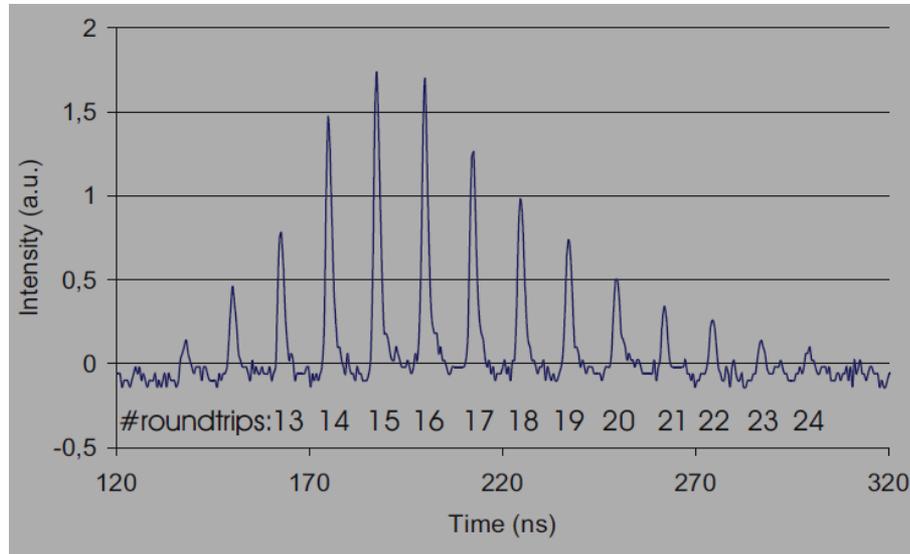
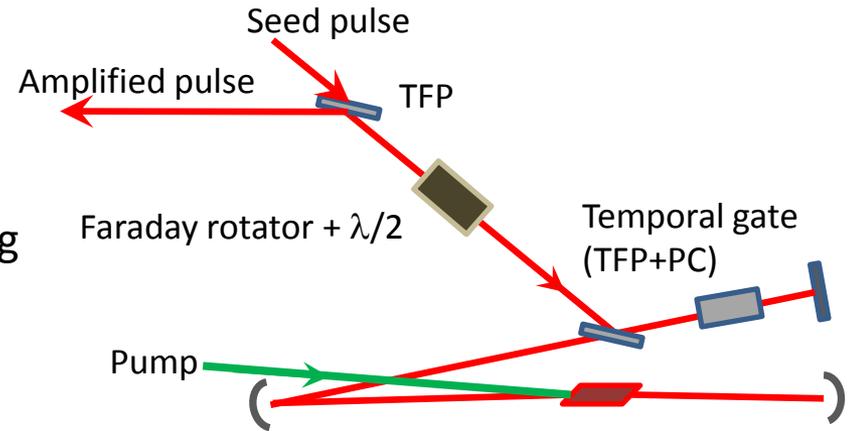
⇒ This requires high optical gain

High average power: up to 5 Watts

Relatively high fluency: $\sim 2 \text{ J/cm}^2$ (far from TiSa damage threshold)

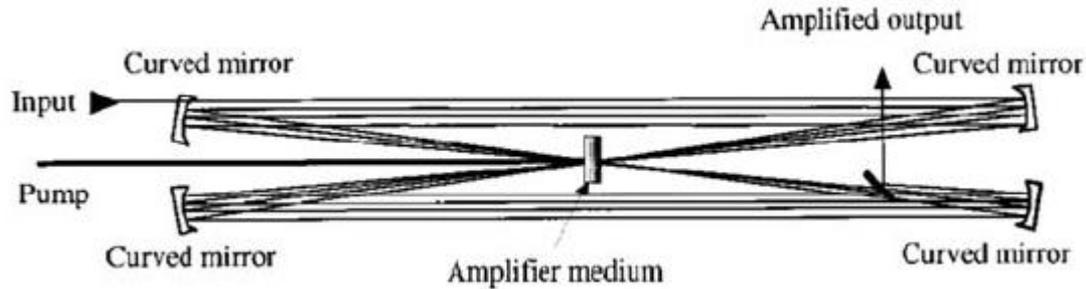
Brewster cut

Water cooling or cryo cooling

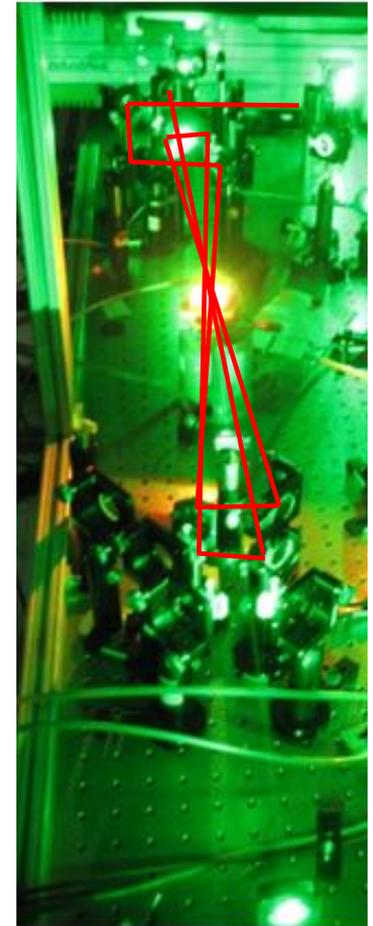


The amplification of femtosecond pulses

In a multipass amplifier:

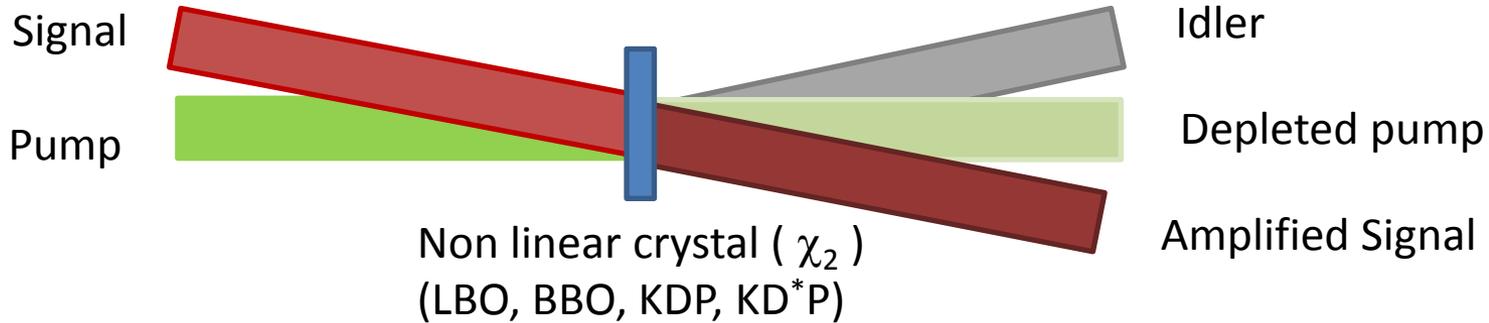


- The population inversion is obtained by one or more “pump lasers” irradiating the TiSa on both sides
- Many passes in the gain medium to extract the deposited energy
- The energy density are:
 - Up to 1.5 to 2 J/cm² for green light
 - Classically up to 2 J/cm² for the red.
- The size of the beam in the crystal can be from 500 μm to 150 mm
- The crystal can be surrounded by:
 - Air when it’s a low rep rate laser and the energy modest (few tens of mJ)
 - Water when the rep rate is at maximum 10 Hz with energy up to few joules
 - Graphite or Indium if it is cryo cooled when the average pump power is > 50 W
 - Index matched liquid when the energy is > 10 joules
- The crystals are AR coated for both spectral bandwidth



The amplification of femtosecond pulses

In a Non collinear Optical Parametric Amplifier:



Benefits	Drawbacks
Single pass design	
NO transverse ASE	Parametric fluorescence
Large spectral bandwidth	Sensitive to angle
Scalable to kJ thanks to crystal size	Dedicated pump lasers Sensitive to intensity on both pump and signal

Can be used either in picosecond or nanosecond regime

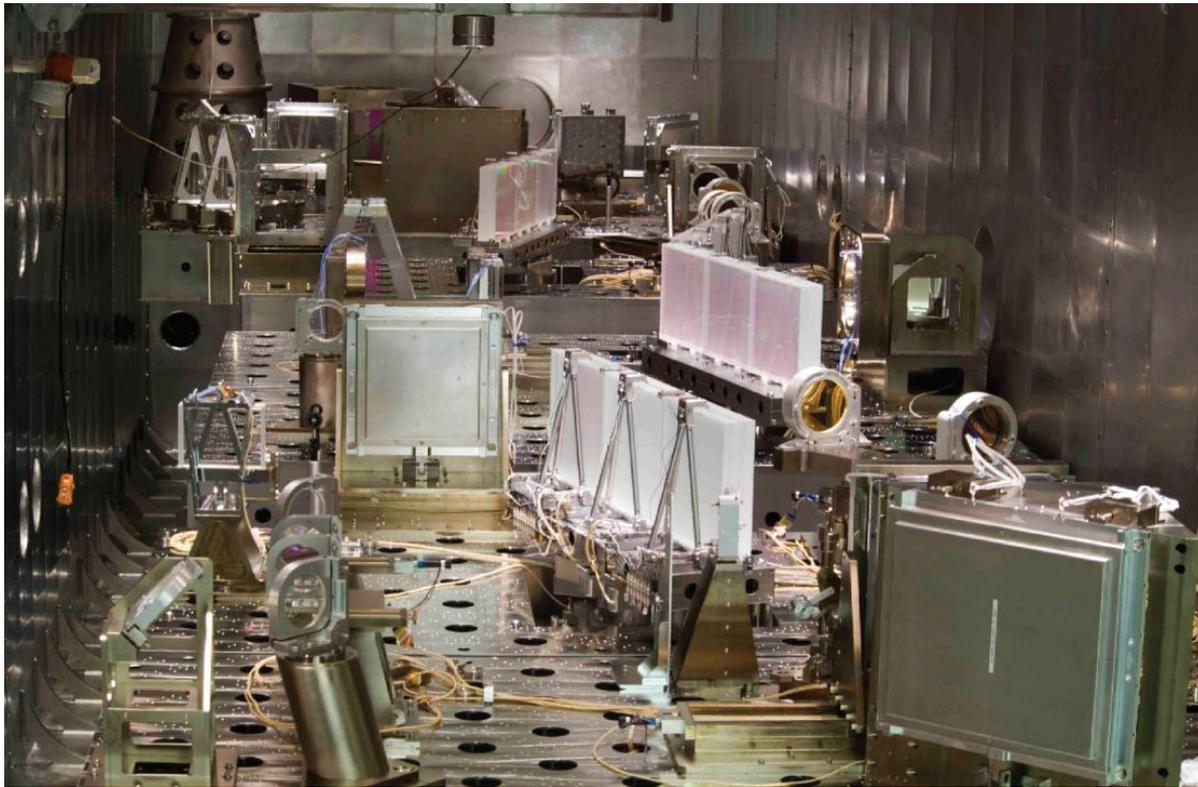
Seed for high energy system (800 or 900 nm)

Energetic Amplification for ultra-short pulses

The compression stage

Due to the very high intensity after compression, propagation in air can not be envisaged
=> under vacuum (10^{-6} mbar)

$$\Delta T = \frac{\phi^{(2)} 4 \ln 2}{\Lambda T} \quad \Phi^{(2)} > 0$$



Omega EP compressor chamber

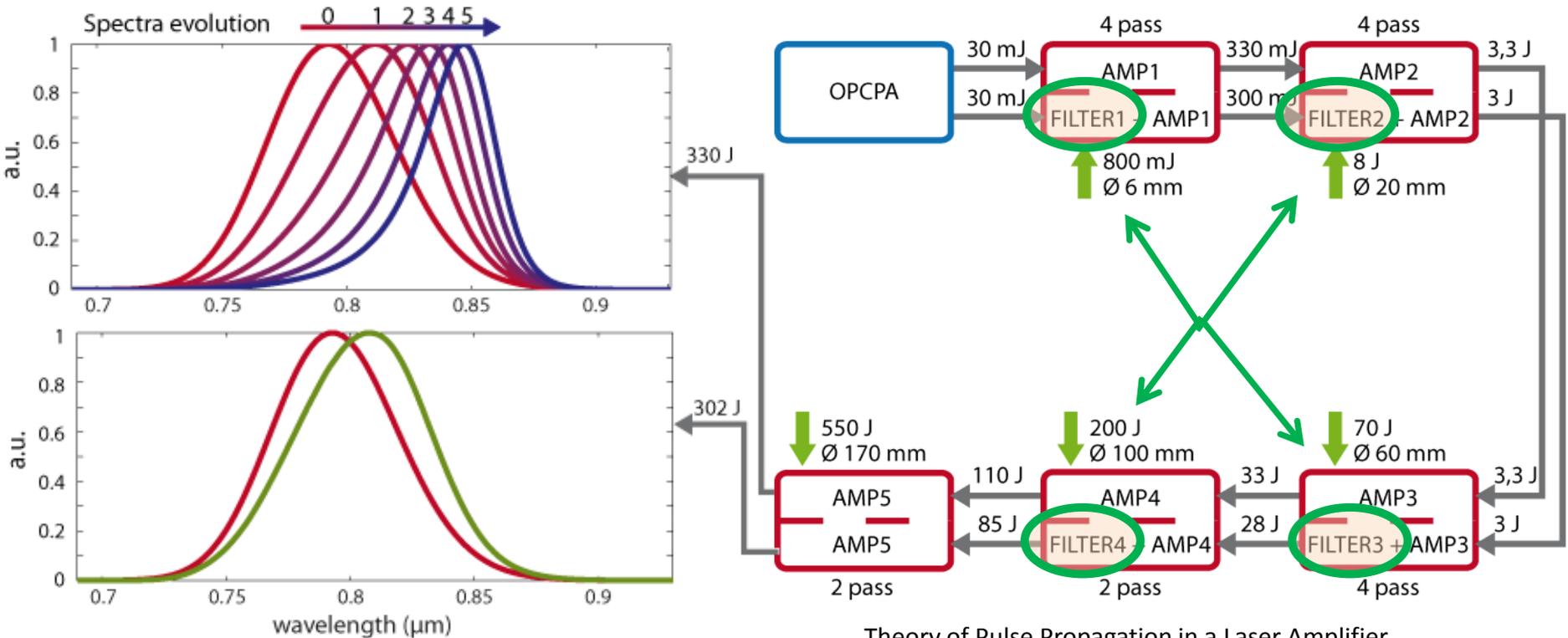
The amplification simulation

The model is based on the **Frantz and Nodvyk** equation for the standard amplification
 The wavelength dependence is obtained thanks to the relation between time and frequency
 as the pulse is temporally chirped

Are taken into account:

- gain cross-section wavelength dependence
- properties of the coatings of the laser components
- losses

Output are: the energy, spectrum and Fourier Transform pulse duration



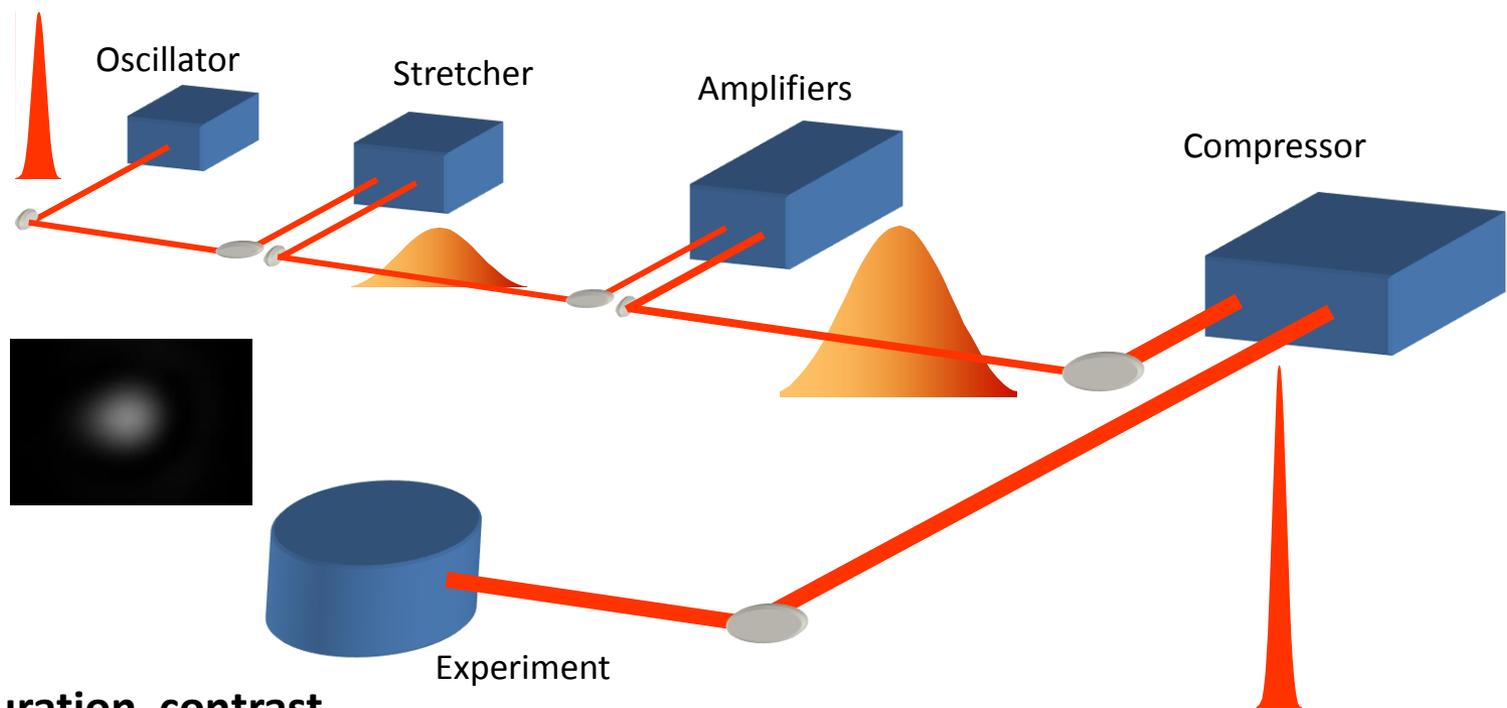
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Characterization of femtosecond intense pulses



Energy

Temporal: duration, contrast

Spatial: focusability

Ideally, measurement of the pulse on-shot in a plane equivalent to the experiment.

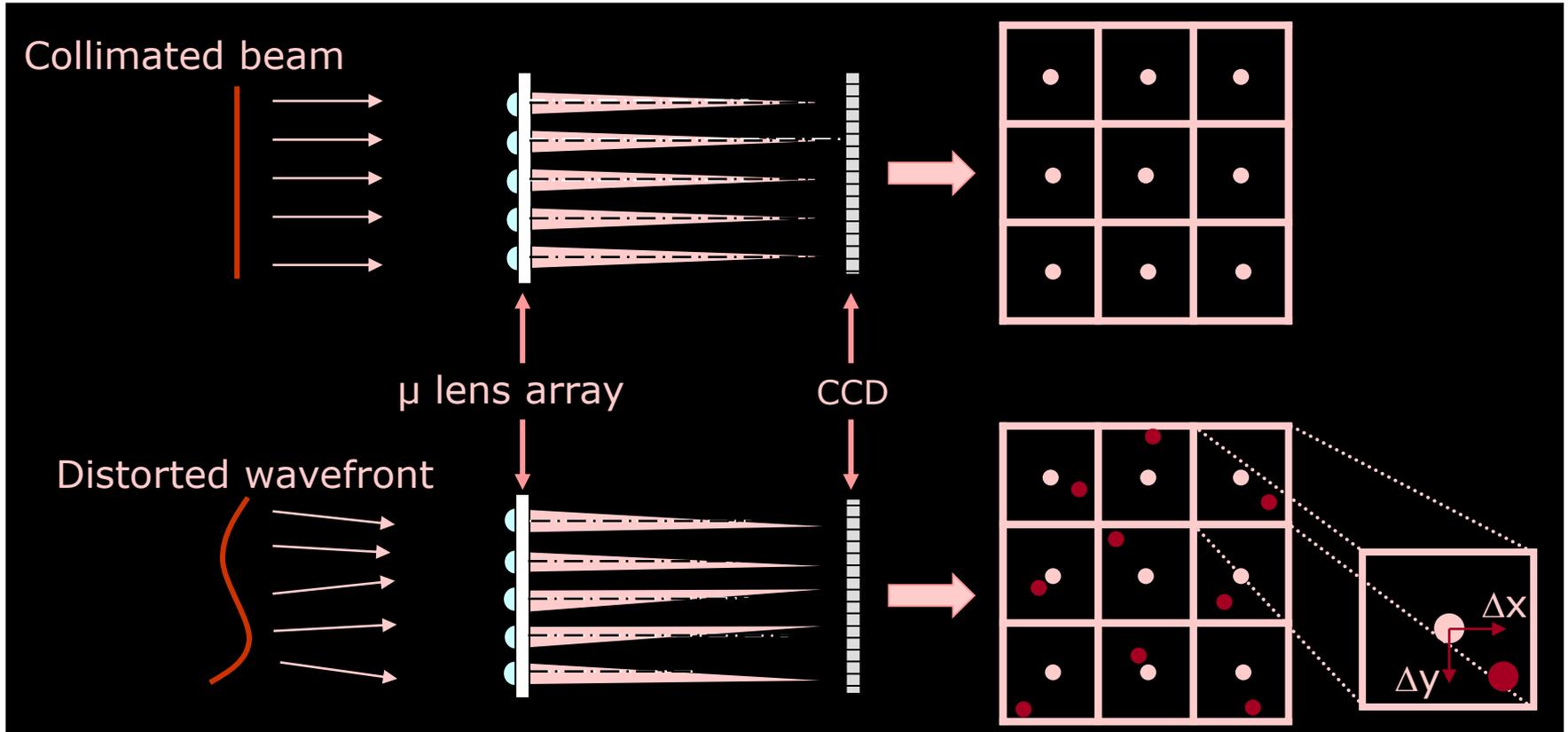
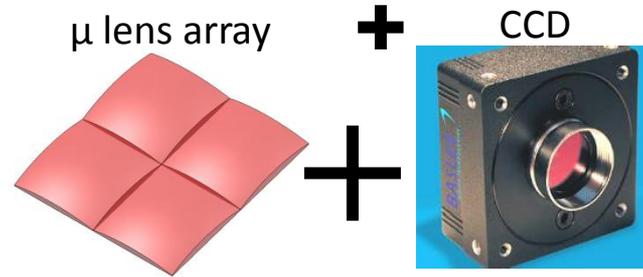
Among difficulties, the main is: HOW TO SAMPLE THE PULSE ?

- ✓ leaky mirror: non linear effects
- ✓ part of the beam: no info on 2D

Usually the pulse is characterized with an attenuated energy

Spatial characteristics measurement

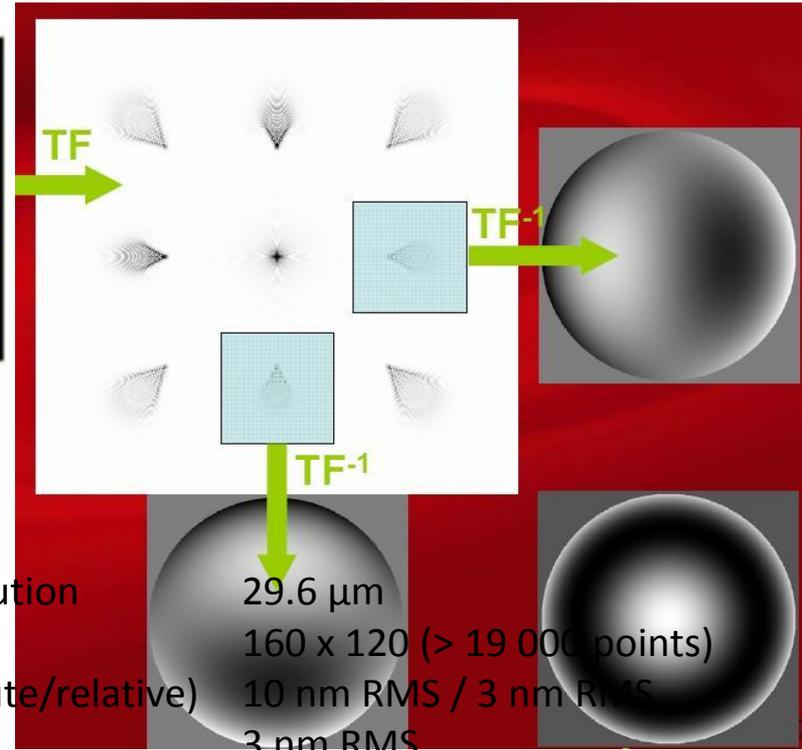
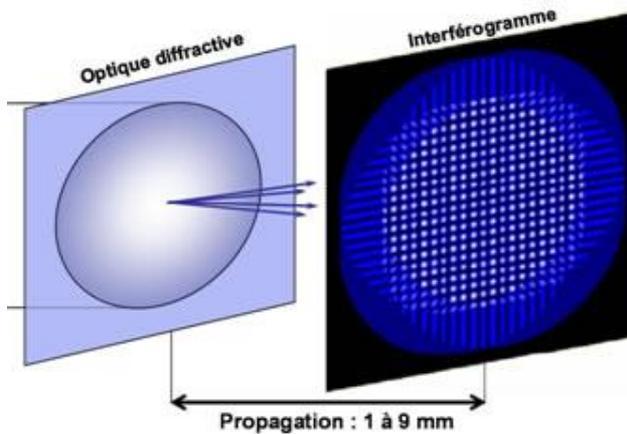
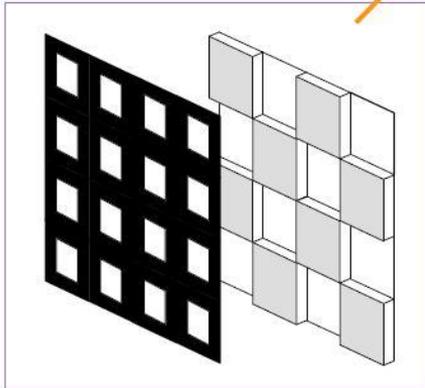
Shack-Hartmann (Imagine Optic, Night N, Adaptive Optic Associates ...)



Spatial characteristics measurement

Lateral shearing interferometer (Phasics/ SID 4)

Based on interferometry



Grid + grating

After the grating, 4 waves are diffracted
They interfere on the CCD chip

Transverse resolution
Sampling
Precision (absolute/relative)
Repeatability
Dynamic

29.6 μm
160 x 120 (> 19 000 points)
10 nm RMS / 3 nm RMS
3 nm RMS
> 100 μm

FFT, spectral filtering and FFT⁻¹
 ⇒ Gradient of the wavefront
 ⇒ Integration
 ⇒ Wavefront

*The edges of the pupil are not measured.
Good transverse resolution*

Spatial characteristics measurement

Based on propagation properties

✓ Phase diversity

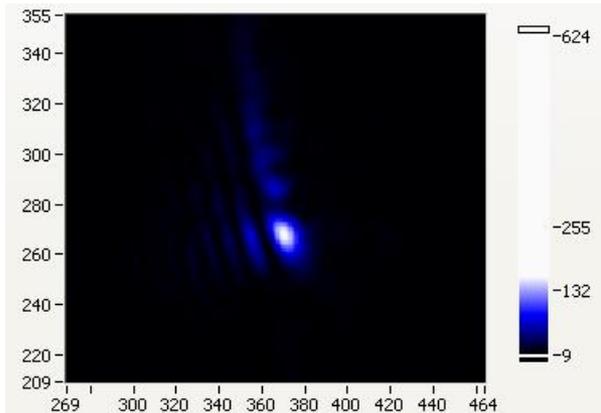
- Measurement of the beam in the focal plane in one or more planes before or after
- There is a unique wavefront for obtaining these patterns

Advantages are:

- Optimizing the beam at focus
- Take into account the aberrations of the transport beam-line

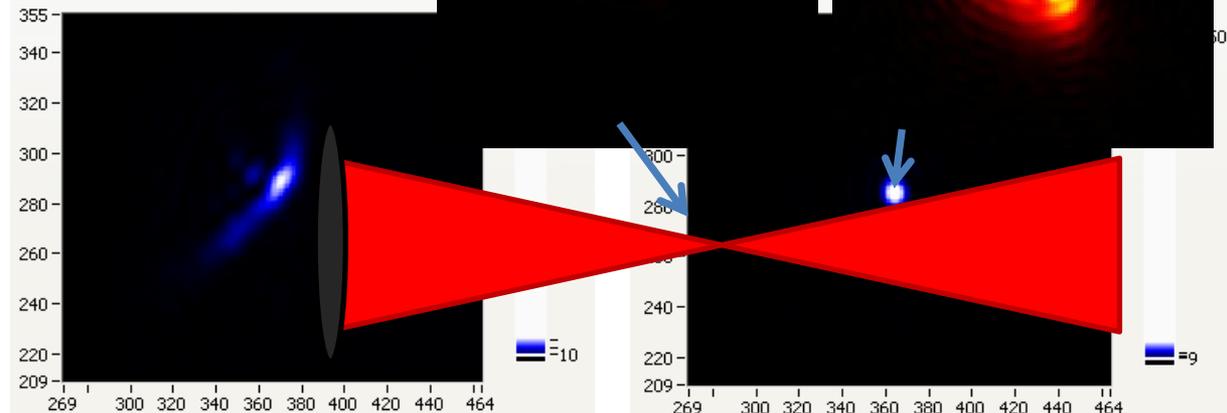
Before adaptative optic:

- 250nm RMS



Standard adaptative optic

- 19nm RMS



Temporal characteristics measurement (duration)

Autocorrelation device

- Michelson interferometer
- 2ω generation
- Detector

Temporal characteristics measurement (duration)

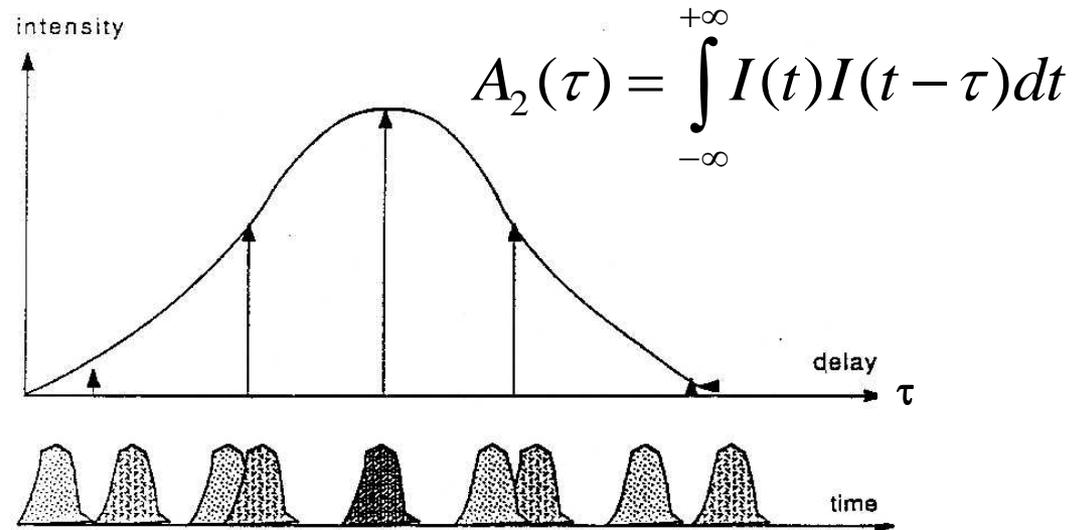
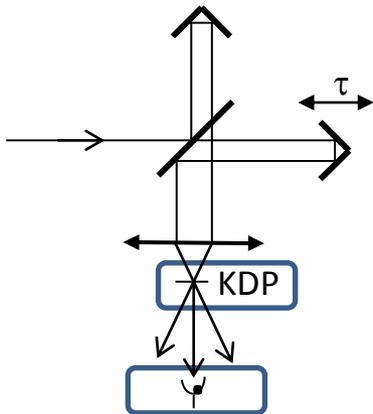
Autocorrelation device

- Michelson interferometer
- 2ω generation
- Detector

Deconvolution factor:

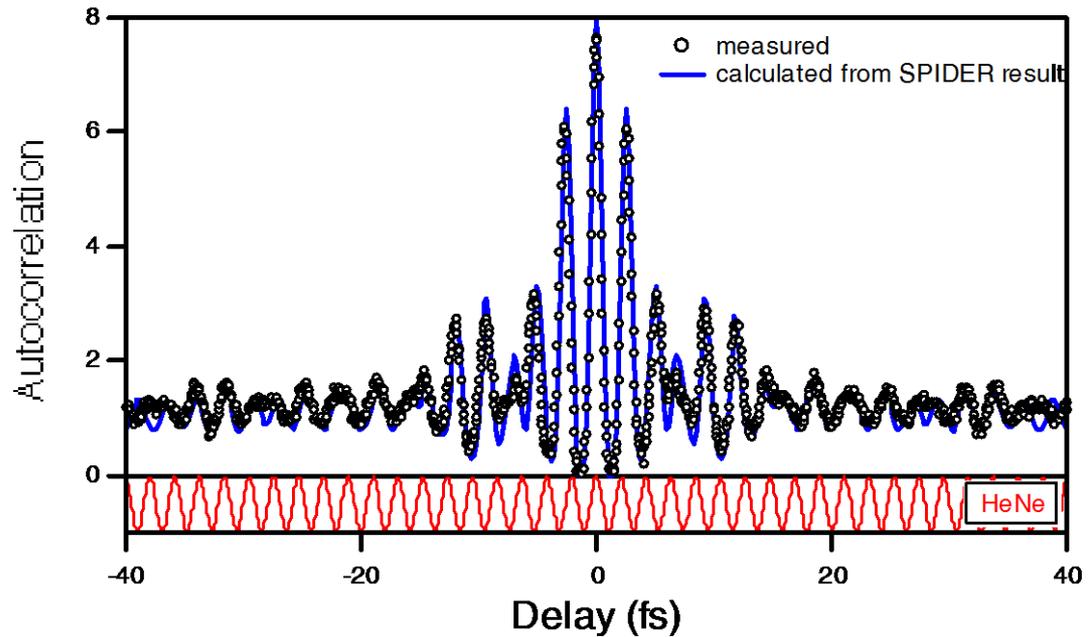
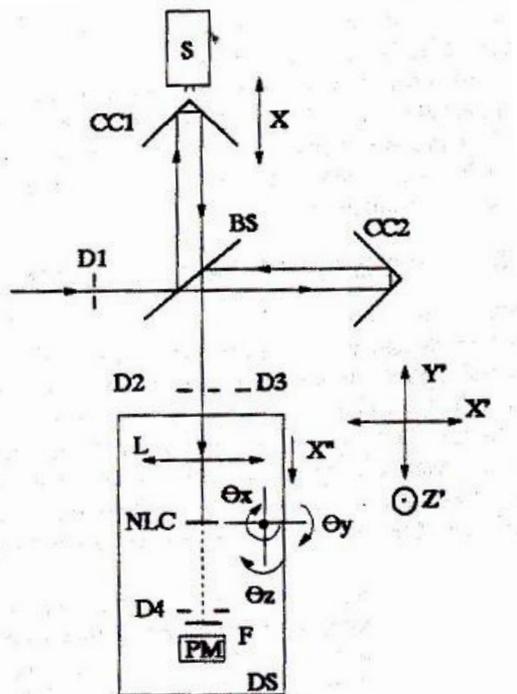
Gaussian: 1.41 (sech)²: 1.55

Background-free correlator



Temporal characteristics measurement (duration)

Interferometric correlator



At $\Delta = 0$, $E_{\text{total}} = E_1 + E_2 = 2E$ si $E_1 = E_2 = \sqrt{I}$. $\rightarrow I_{\text{fondamental}} \propto 4 E^2 \rightarrow I_{2\omega} \propto 16 I^2$

At $\Delta = \infty$, $I_{\text{fondamental}} = 2 \sqrt{I} \rightarrow I_{2\omega} \propto 2 I^2$

So $S_0/S_\infty = 8$

Both correlator does not give access to the pulse temporal profile

Temporal characteristics measurement (duration)

Pulse characterization \Leftrightarrow phase (temporal or spectral) measurement

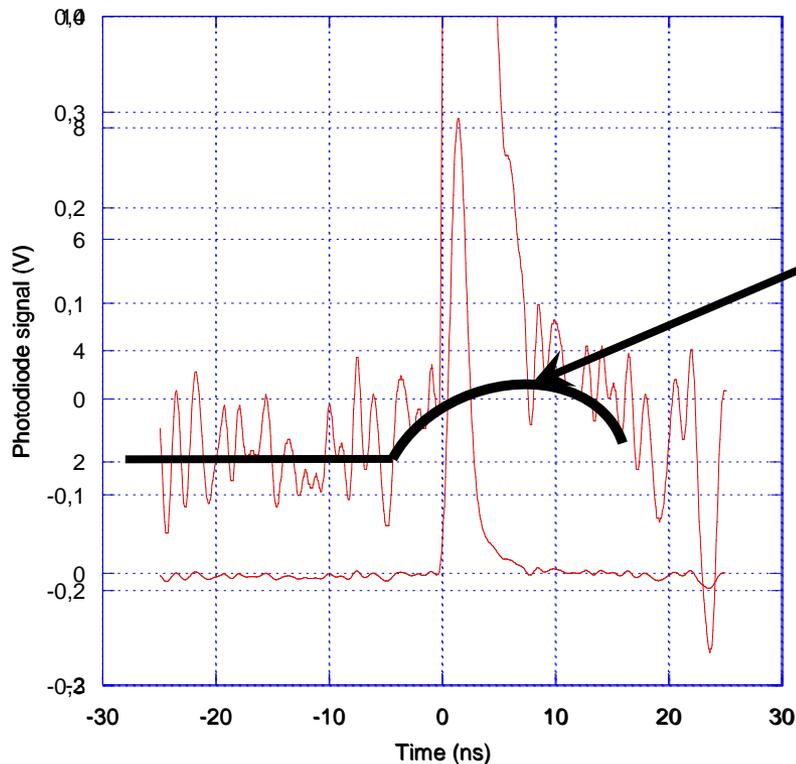
It requires a non linear effect if no reference pulse is used

FROG/GRENOUILLE	SPIDER	WIZZLER	D-Scan
Spectrometric approach	Interferometric approach		Spectrometric approach
Single shot			
2D	2D	1D	1D
Iterative algorithm	FFT calculations	Iterative algorithm	2 nd ω theory
Info on the trace	No info on the trace	No info on the trace	No info on the trace
No info on the edges	No info on the edges	Good info on the edges	Info on the edges
Difficult at focus	Not at focus	Possible at focus	Possible at focus
			Demonstration under vacuum

Temporal characteristics measurement (contrast)

The temporal contrast is a key parameter for achieving controlled experimental conditions.

A simple way to measure on a long time scale the nanosecond contrast, is the use of a fast oscilloscope together with a fast photodiode or photoconductor switch and calibrated neutral filters



Fluorescence background

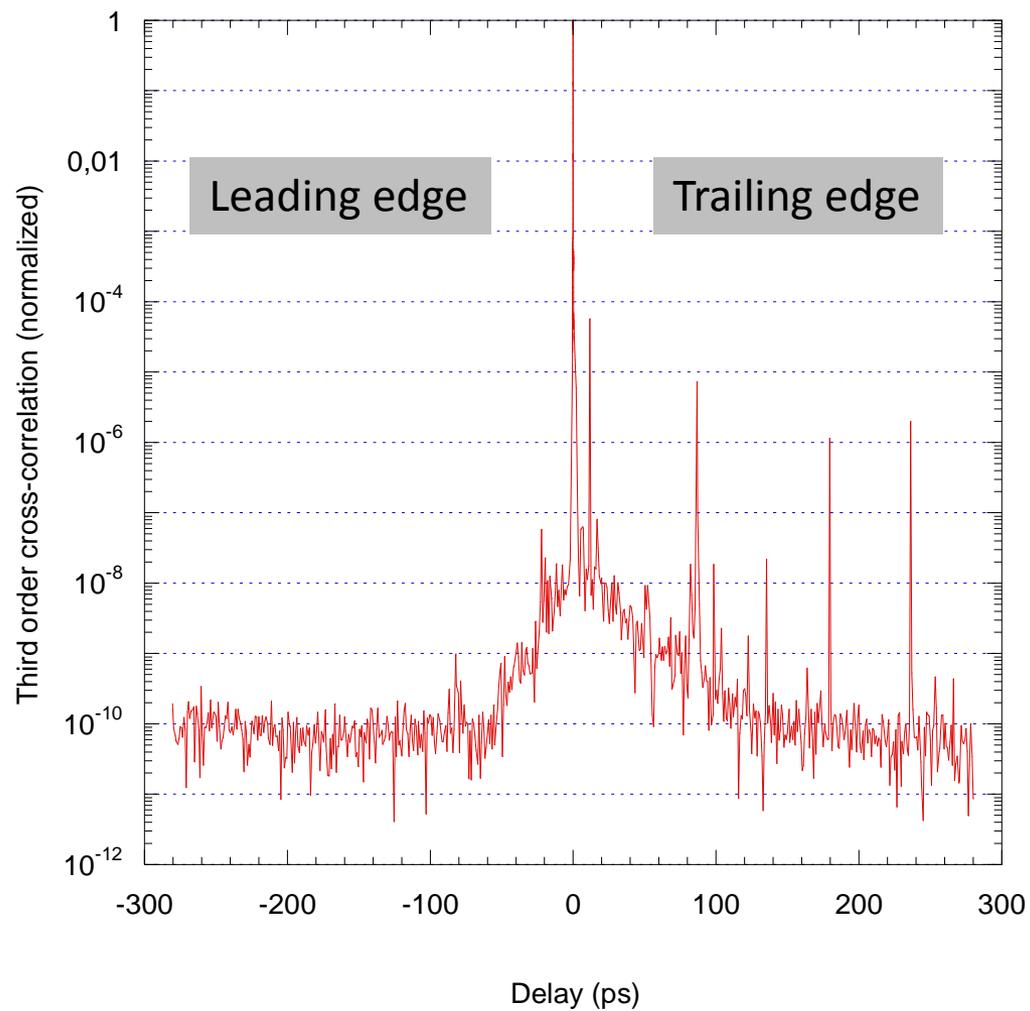
$$V_{\text{peak}}/V_{\text{fluo}} = 160$$

Ratio of the final pulse durations = 2 ns vs 20 fs

Estimated ns contrast : $\sim 6 \cdot 10^{-8}$

Temporal characteristics measurement (contrast)

High dynamics correlation typical trace on a 10 Hz system at 2 joules per pulse



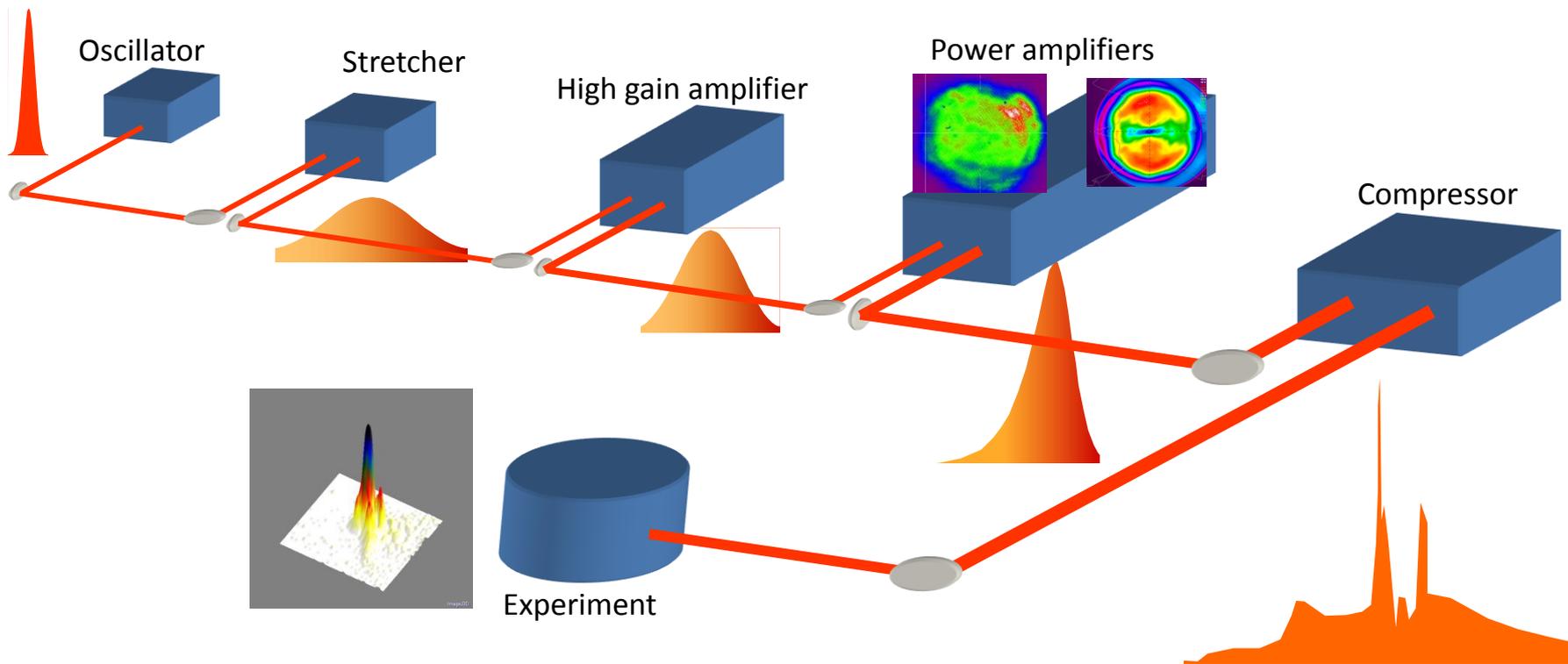
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The different issues on high energy and short pulses duration lasers



Limited spectral bandwidth and aberrations temporal profile degradation

Spectral gain narrowing, ASE => \uparrow duration and \downarrow temporal contrast

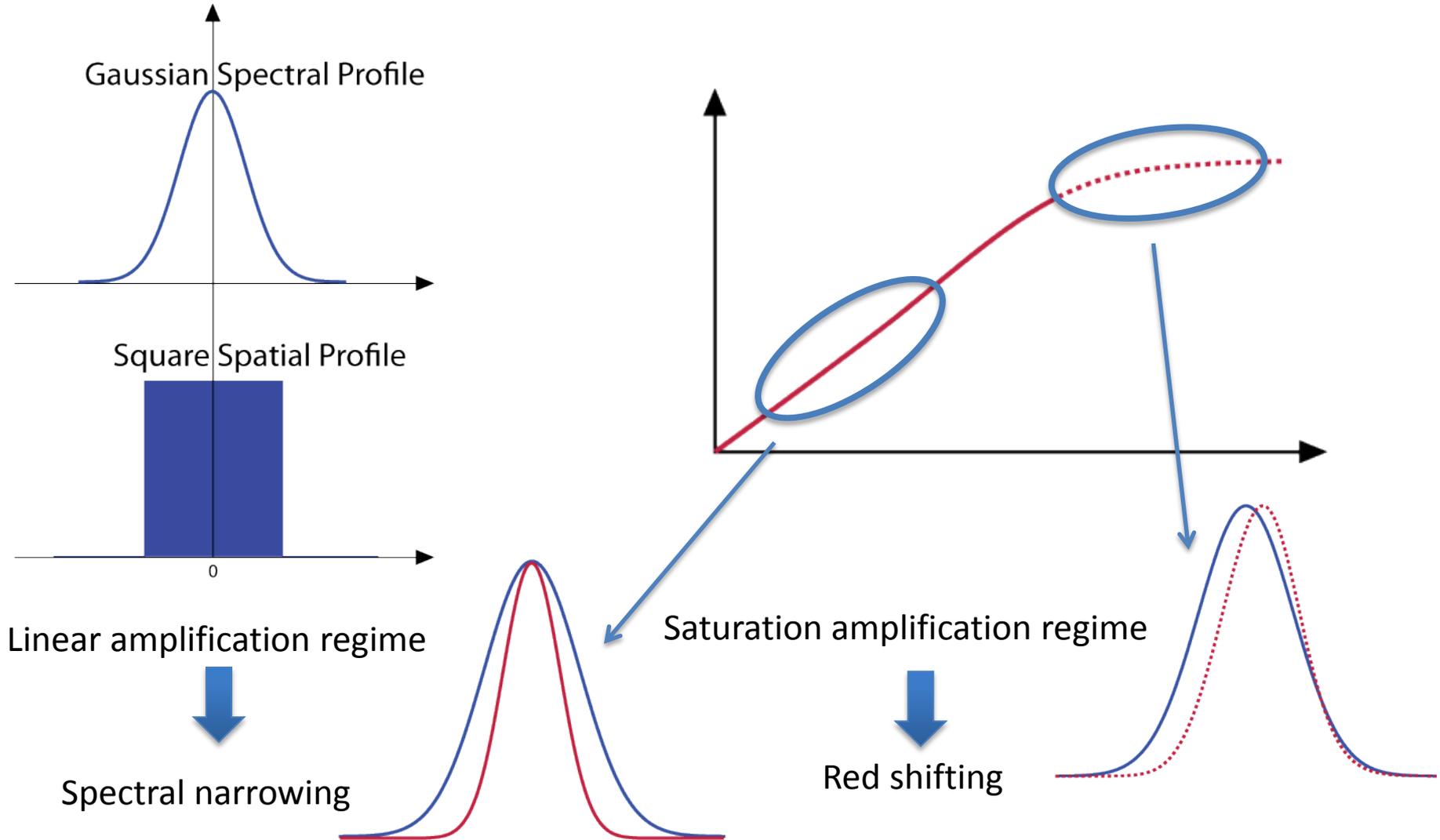
Spectral shifting, pump laser spatial profile, transverse lasing => \uparrow duration, degraded beam and \downarrow energy

Temporal phase defaults => temporal pulse profile degraded

Wavefront distortions=> lower intensity



Spectral distortions with amplification



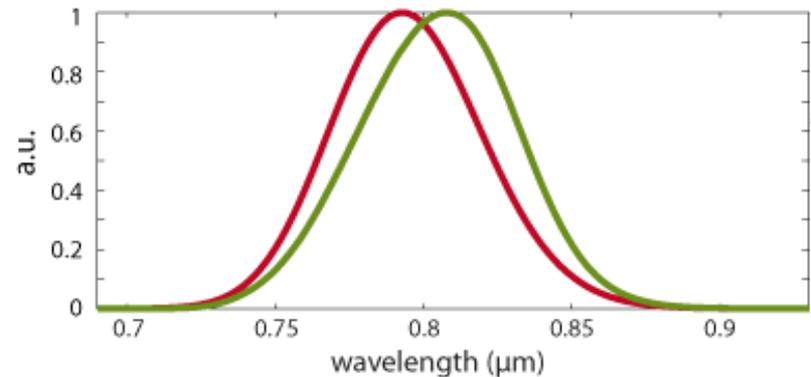
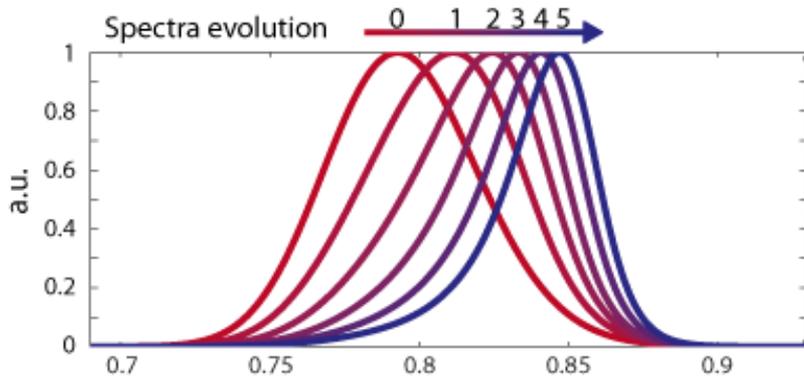
These changes induce pulse duration broadening and temporal profile distortions.

Spectral distortions with amplification: The solutions

Spectral filtering is used to pre or compensate the amplification effects

- Mirror with variable reflectivity:
 - Gaussian shape for gain narrowing only
 - Dedicated shape for pre-compensating gain narrowing and shifting
- AOPDF (Mazzler) in regenerative cavity

The other solution is to replace the TiSa amplifier by OPCPA stage

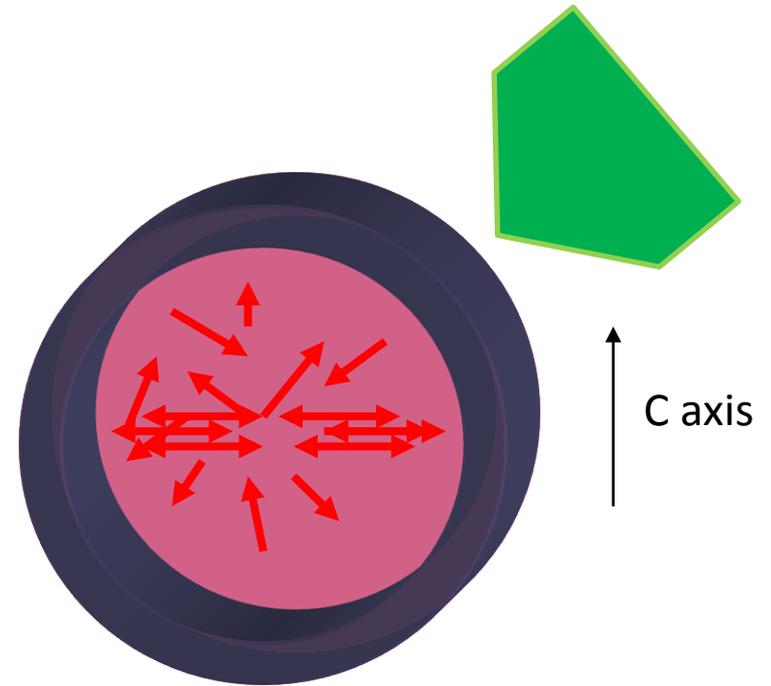
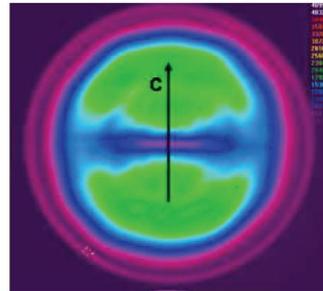


The parasitic effects in large crystals (> several cm diameter)

There are two effects:

- **Transverse lasing**

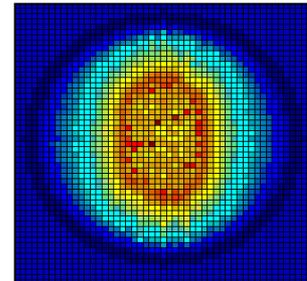
This is due to oscillation in the crystal due to reflections on the edges of the crystal



- **ASE depletion**

This is unavoidable.

To reduce it, a low doping level is required

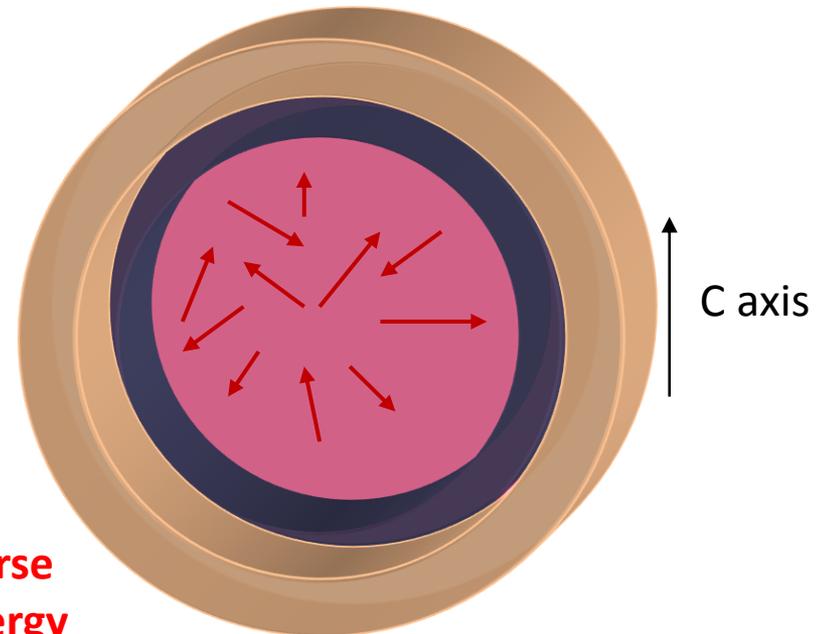


The parasitic effects in large crystals: Solution

- Low doping level
- Polished periphery
- Absorbing material around the crystal
 - Index matched liquid
 - Solid material
 - Ti^{4+}

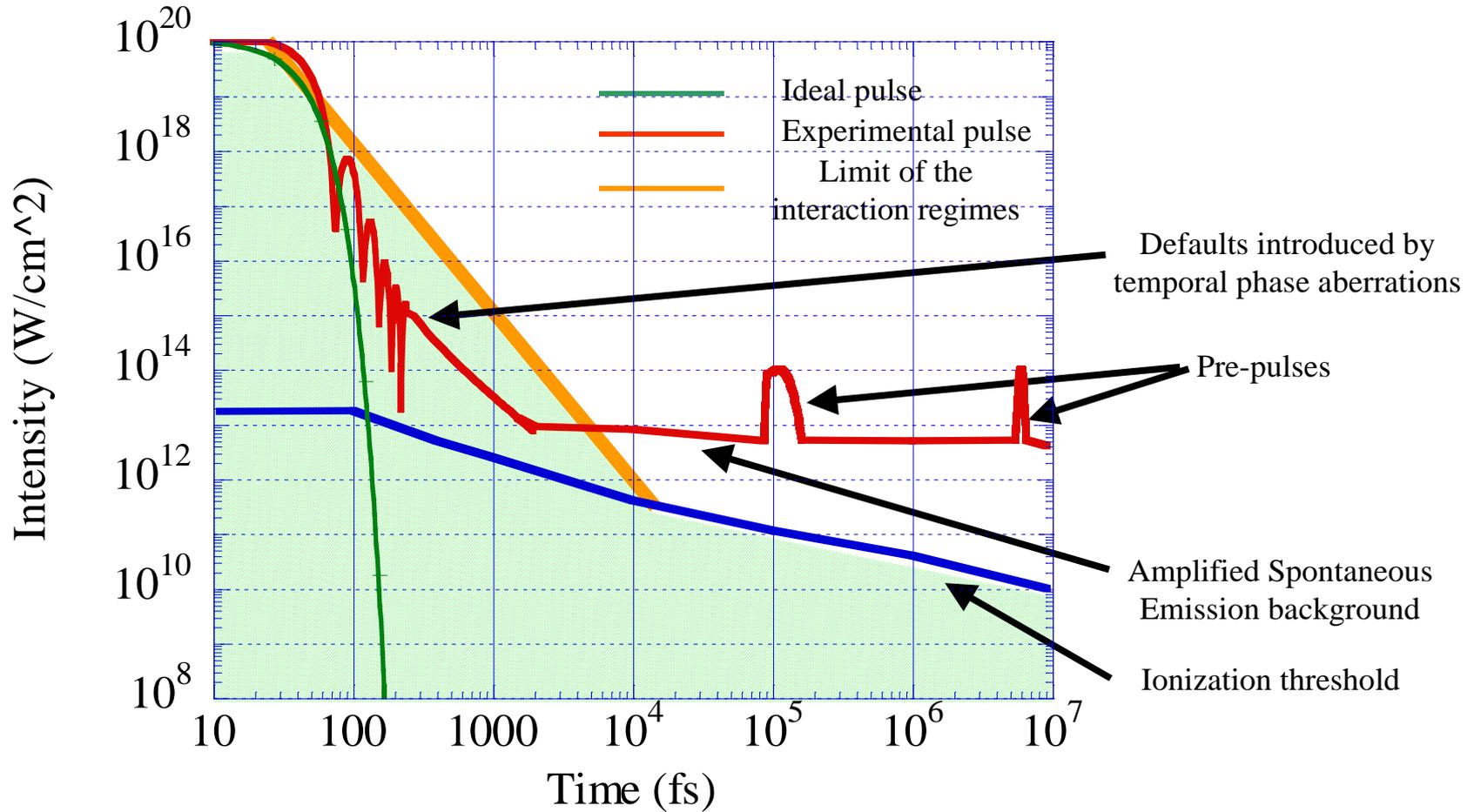
Index-matched liquid (diiodomethane – CH_2I_2) mixed with a dye absorbing 800 nm light. This liquid will be circulating around the crystal periphery for ensuring good homogeneity of the mixture

Some characteristics of CH_2I_2	
Refractive index at 589,3 nm	1,7425 ^[1]
Melting temperature	6°C
Boiling temperature	181°C



With a proper mixture, no transverse effect with 330 Joules pumping energy demonstrated

Temporal characteristics degradation



Coherent contrast: spectral clipping, spectral phase errors
Incoherent contrast: ASE pedestal

Temporal contrast degradation

Defect of the spectral phase

- Presence of large amount of material leads to residual GDD

The solutions are:

- Use some static correction: prism line, Chirped mirrors
- Use controllable tools: SLM in a 0 delay line, AOPDF (Dazzler)

ASE background

- In TiSa amplifier with high gain, generation of nanosecond background of ASE.
The level for mJ pulse can be 10^{-9} relatively to the peak power.

This pedestal is far not low enough for high intensity experiment.

The solutions are:

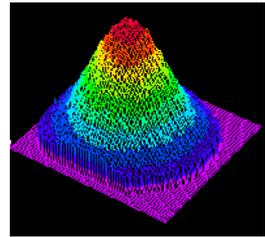
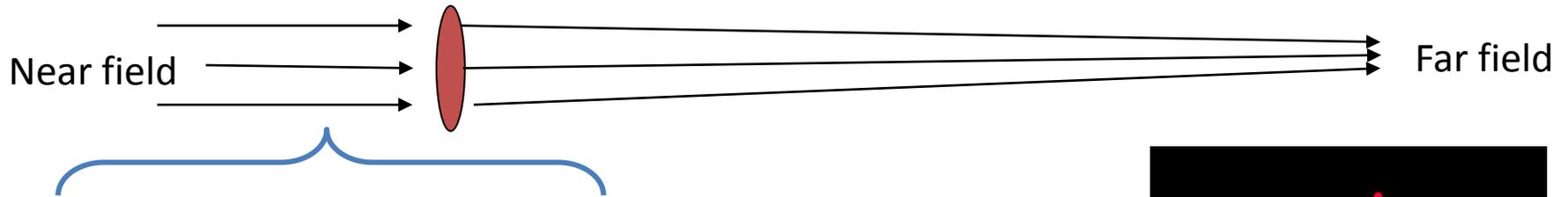
- Replace TiSa amplifier by picosecond OPCPA
- Implement ASE filtering in a double CPA configuration (Saturable absorber, XPW)
- Plasma mirrors before experiment

Spatial degradations

$$I \text{ (W/cm}^2\text{)} = E \text{ (Joule)} / \Delta t * S \rightarrow \text{cm}^2$$

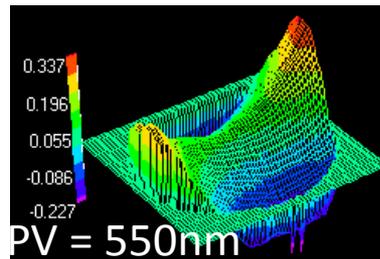
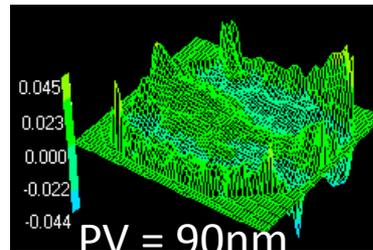
$$S \propto \frac{\lambda f}{D}$$

Depends on wavefront
At focus



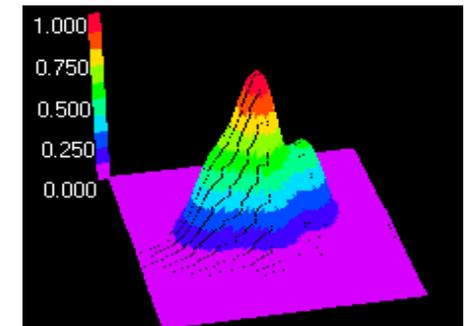
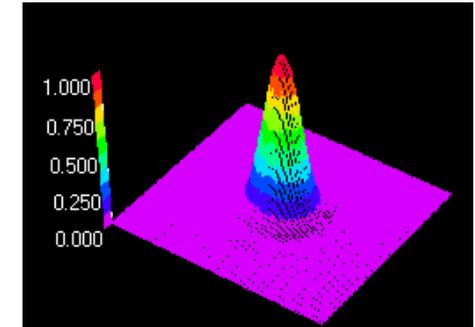
Beam profile

+



Wavefront

Focusing



•The focal spot size has increased.

➤ the intensity is lower

Spatial degradations: causes

For PW class Lasers :

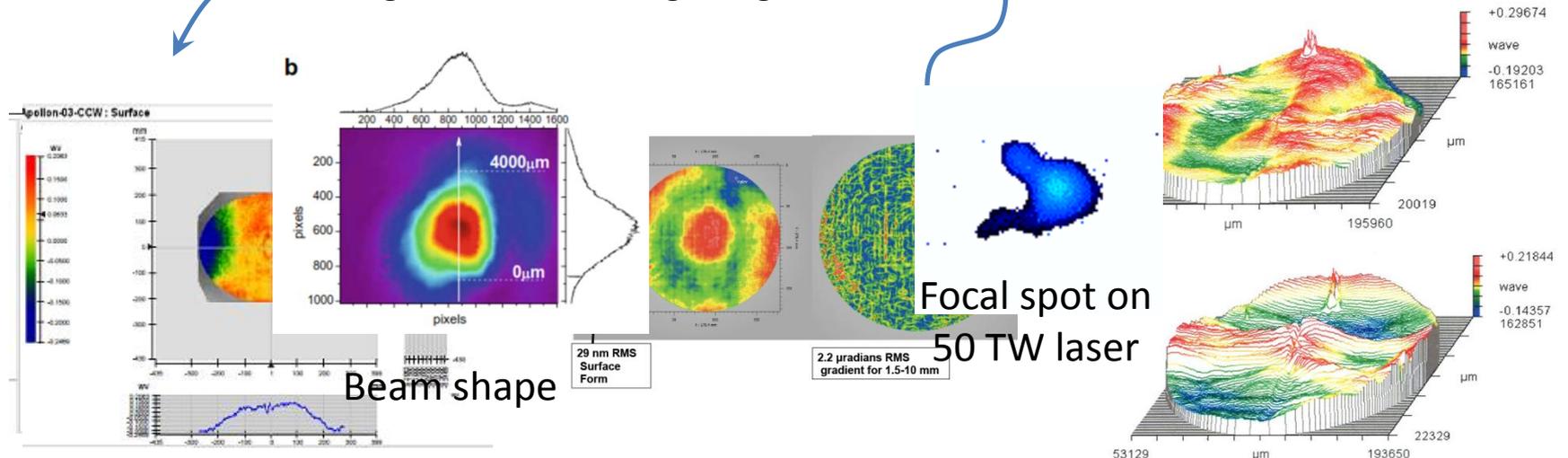
~200 components

beam propagation : 300 - 400 meters

- beam profile deformation
- wavefront distortions

➤ Origins :

- Laser process; amplification (pump laser beam profile), thermal effects => $A(x,y)$ and $\phi(x,y)$
- Aberrations due to optical design : spherical, astigmatism, curvature => $\phi(x,y)$
- Large components defaults : low and high spatial frequencies => $A(x,y)$ and $\phi(x,y)$
 - Laser media; Large size crystals
 - Large size mirrors (up to 650 mm)
 - Large size diffraction gratings



Spatial degradations: quantification

Strehl ratio quantifies the degradation

$$SR = \frac{\textit{ExperimentalIntensity}}{\textit{referenceIntensity}}$$

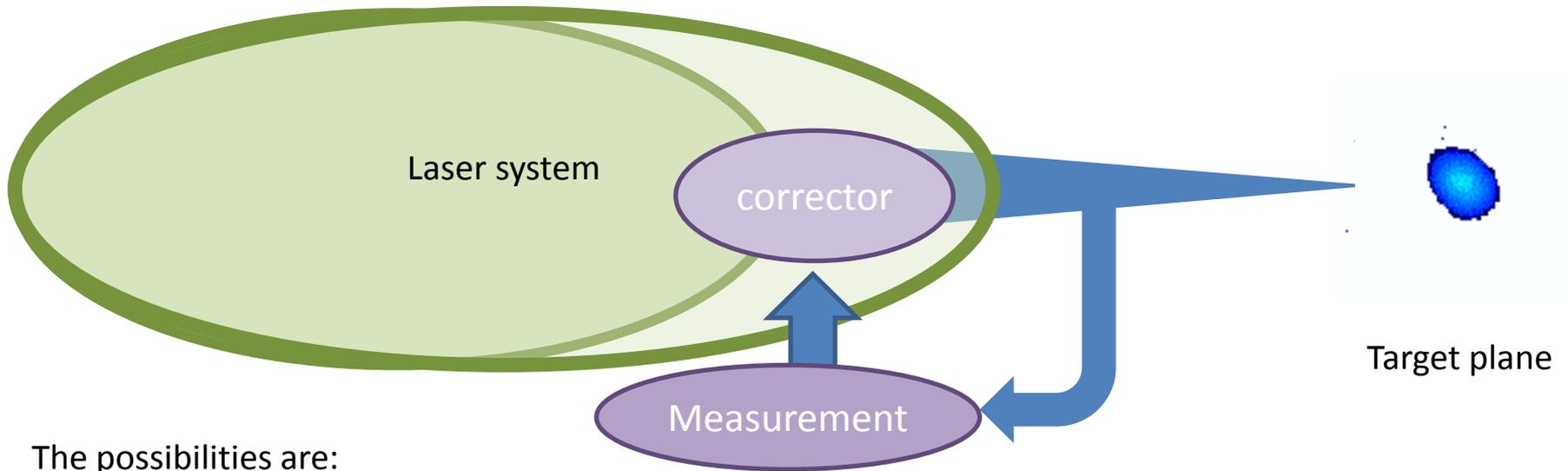
Experimental beam and wavefront.

Reference beam and plane wavefront

1. For astronomy, the energy is uniform in the pupil
2. For laser it can be relevant to choose another one.
 - gaussian or experimental

Spatial degradations: solutions

Corrections of the wavefront distortions



The possibilities are:

- **Spatial filter**

- + inside the global laser set-up
- + remove high spatial frequencies
- damage threshold then destruction

- **Optic valves**

- + high spatial frequencies
- low damage threshold

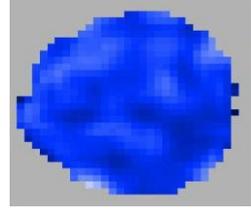
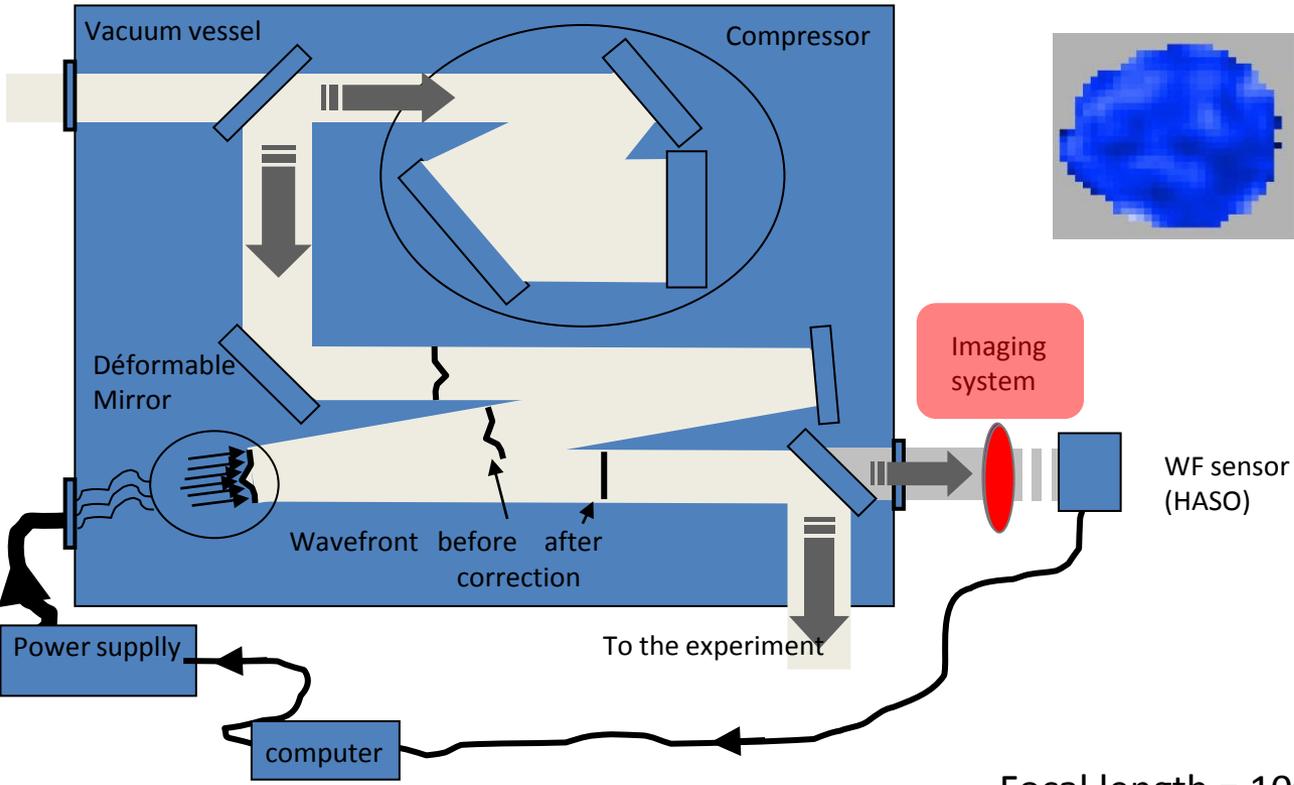
- **Deformable mirrors**

- + high damage threshold
- + large size
- low spatial frequencies

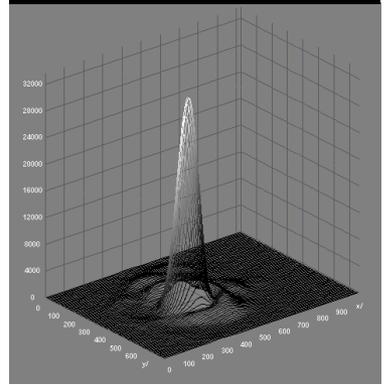
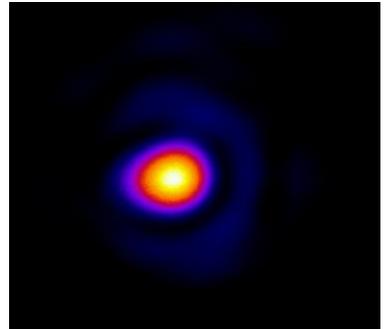
A combination of both seems to be the relevant solution

Different results obtained on ~100 TW laser beams

For **100 TW at LOA (2.5 J in 25 fs)** : after compression
The DM is a monomorph type (CILAS)



23 nm rms, 211 nm PV
Measurement 32x32 points



WF sensor (HASO)

Focal length = 1000 mm
 μ scope objective : x 20
12 bits CCD

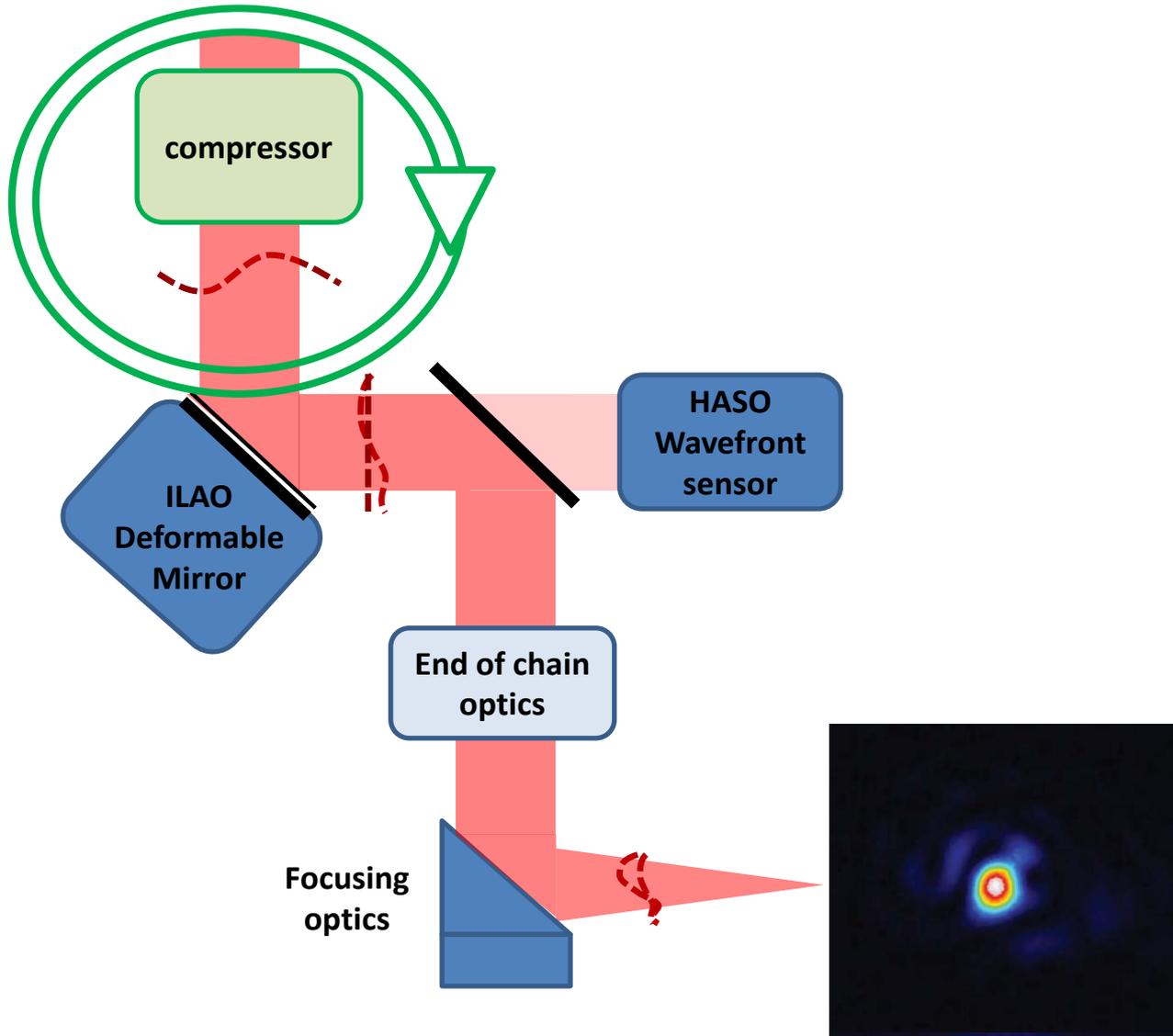
Single shot correction

Strehl ratio > 0,9

Different results obtained on ~100 TW laser beams

On UHI-100 at CEA Saclay (2.5 J in 25 fs) : after compression

The DM is baser on the use of mechanical actuators

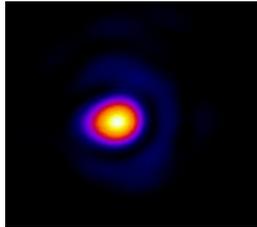
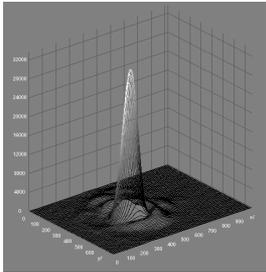


The limitations the actual corrections for high intensity laser beams

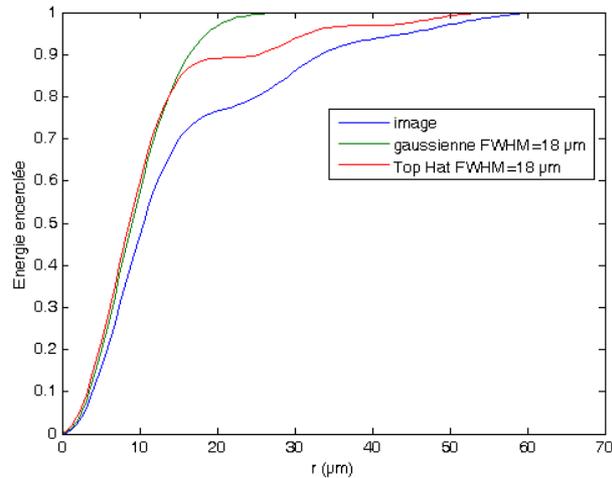
Beam shape modulations are limiting the far-field quality.

Measurement on 100 TW laser

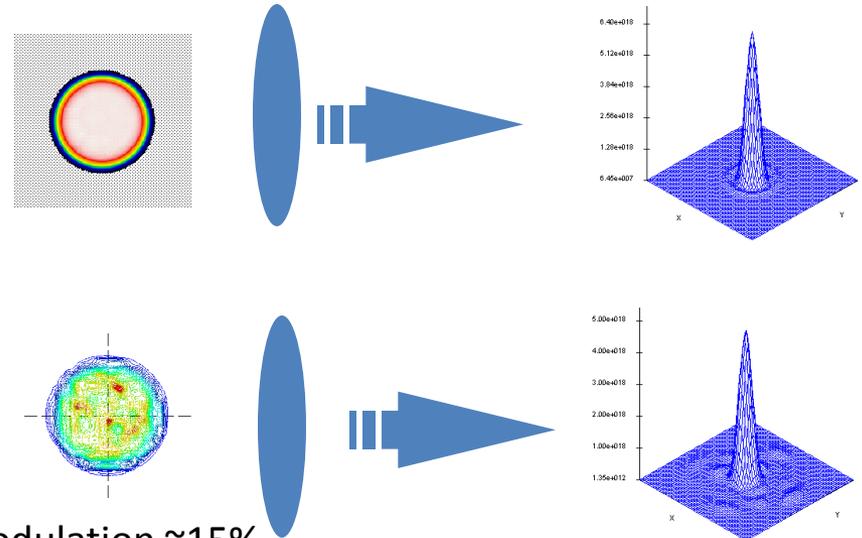
Focal spot



Encircled energy



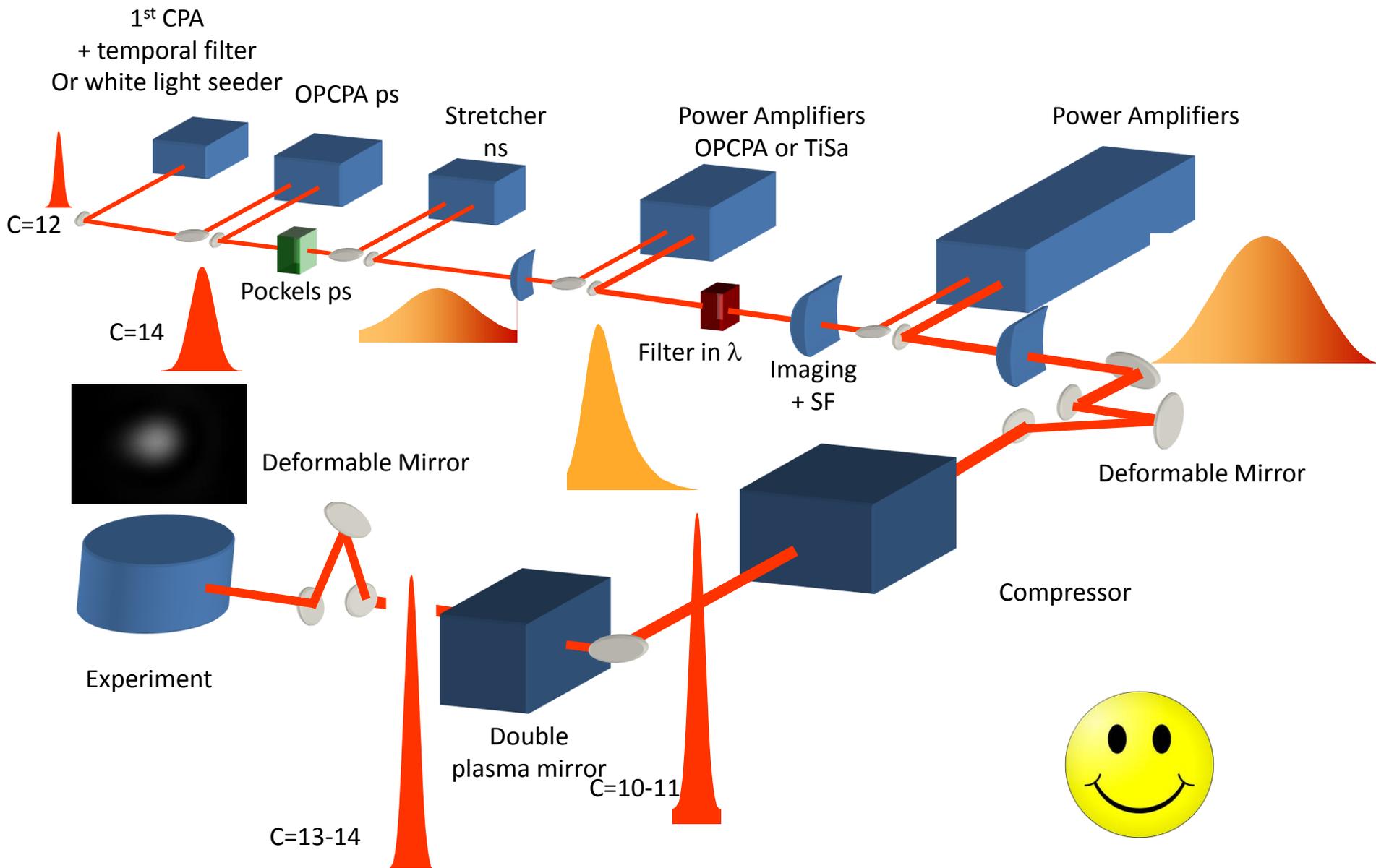
72% of the energy is in the main peak.
To be compared to 88% for a « top hat »



The **limitation** is no more the spatial phase but **the energy distribution**

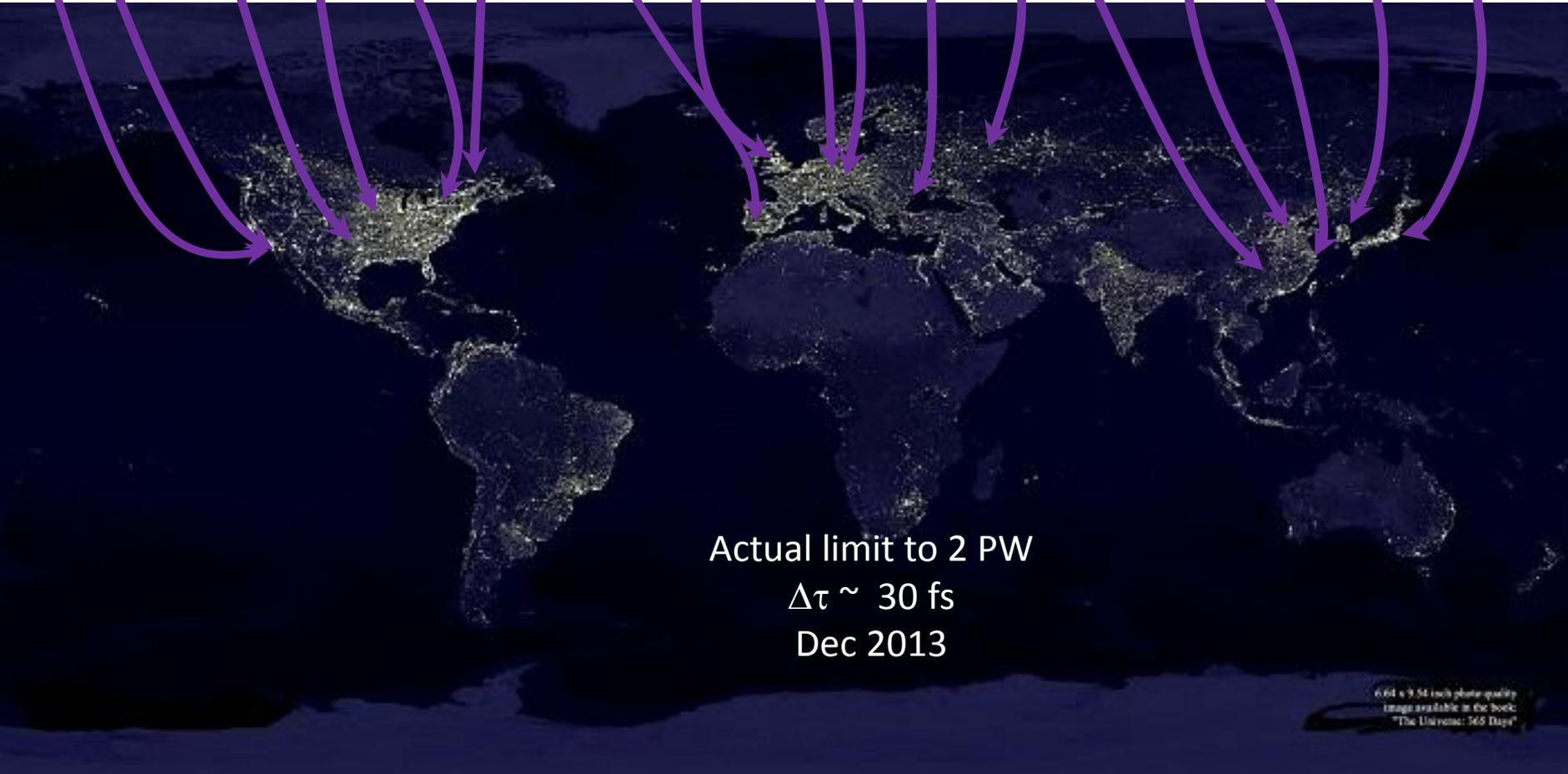
➤ to be controlled by the use of multi-conjugated AO

The new architecture for achieving multi PW pulses



Intense laser systems with potential intensity higher than $10^{20} - 10^{21} \text{ W/cm}^2$

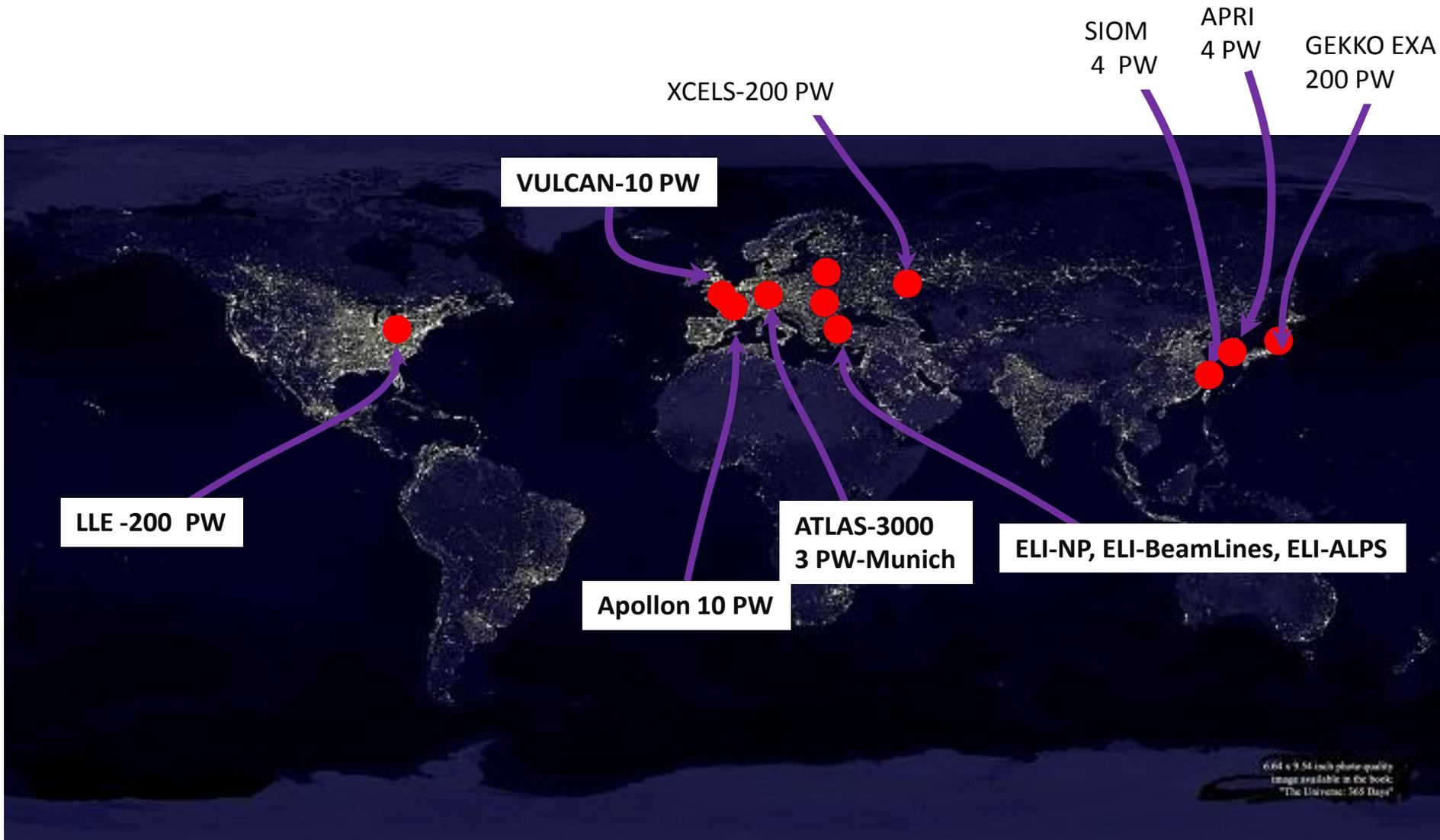
- BELLA 1.3 PW
- LLNL 0.3 PW
- Texas PW 1 PW
- UNL 1 PW
- Hercules 0.3 PW
- ALLS 0.2 PW
- Astra-Gemini 2*0.5 PW
- Salamanca 1PW DRAGO
- Jena 0.5 PW
- Dresden 0.5 PW
- Pearl 0.6 PW
- INLFPR 1 PW
- SILEX 0.3 PW
- Beijing 1.2 PW
- SIOM 2 PW
- APRI 1+1.5 PW
- J-KAREN 0.5 PW



Actual limit to 2 PW
 $\Delta\tau \sim 30 \text{ fs}$
Dec 2013

6.64 x 9.54 inch photo quality image available in the book: "The Universe: 365 Days"

MORE PW
 $\Delta\tau \sim 15 - 30 - 150 \text{ fs}$?



CONCLUSION

10 PW is the actual target for many projects

- **Different techniques are used: TiSa, Nd:Gass or KDP**
- **Most issues have been solved for reaching the peak intensity with good characteristics**
- **Demonstration on operation will have to be demonstrated**

- **The main challenge remains on the measurement of the final pulse characteristics ON SHOT**